## ME:5160 (58:160) Intermediate Mechanics of Fluids Fall 2022 - HW5 Solution

P3.77 Water at $20^{\circ} \mathrm{C}$ flows steadily through a reducing pipe bend, as in Fig. P3.77. Known conditions are $p 1=350 \mathrm{kPa}, D 1=25 \mathrm{~cm}, V 1=2.2 \mathrm{~m} / \mathrm{s}, p 2=120 \mathrm{kPa}$, and $D 2=8$ cm . Neglecting bend and water weight, estimate the total force which must be resisted by the flange bolts.


Solution: First establish the mass flow and exit velocity:

$$
\dot{\mathrm{m}}=\rho_{1} \mathrm{~A}_{1} \mathrm{~V}_{1}=998\left(\frac{\pi}{4}\right)(0.25)^{2}(2.2)=108 \frac{\mathrm{~kg}}{\mathrm{~s}}=998\left(\frac{\pi}{4}\right)(0.08)^{2} \mathrm{~V}_{2}, \quad \text { or } \quad \mathrm{V}_{2}=21.5 \frac{\mathrm{~m}}{\mathrm{~s}}
$$

The CV surrounds the bend and cuts through the flanges. The force balance is

$$
\begin{aligned}
& \sum \mathrm{F}_{\mathrm{x}}=-\mathrm{F}_{\text {bolts }}+\mathrm{p}_{1, \text { gage }} \mathrm{A}_{1}+\mathrm{p}_{2, \text { gage }} \mathrm{A}_{2}=\dot{\mathrm{m}}_{2} \mathrm{u}_{2}-\dot{\mathrm{m}}_{1} \mathrm{u}_{1}, \quad \text { where } \mathrm{u}_{2}=-\mathrm{V}_{2} \text { and } \mathrm{u}_{1}=\mathrm{V}_{1} \\
& \text { or } \mathrm{F}_{\text {bolts }}
\end{aligned}=(350000-100000) \frac{\pi}{4}(0.25)^{2}+(120000-100000) \frac{\pi}{4}(0.08)^{2}+108(21.5+2.2) .
$$

P3.94 A water jet 3 inches in diameter strikes a concrete $(\mathrm{SG}=2.3)$ slab which rests freely on a level floor. If the slab is 1 ft wide into the paper, calculate the jet velocity which will just begin to tip the slab over.


Fig. P3.94

Solution: For water let $\rho=1.94$ slug/ $\mathrm{ft}^{3}$. Find the water force and then take moments about the lower left corner of the slab, point B. A control volume around the water flow yields
$\sum F_{x}=F_{\text {onjet }}=\Sigma n_{\text {out }} u_{\text {out }}-\Sigma h_{\text {sin }} u_{\text {in }}=n k_{\text {out }}(0)-\rho A V(-V), \quad F=\rho A V^{2}$
$\sum M_{B}=\left(\rho A V^{2}\right)\left(\frac{21.5}{12} f t\right)-W_{\text {slab }}\left(\frac{4}{12} f t\right), W_{\text {slab }}=(2.3 \times 62.4)\left(\frac{8}{12} f t\right)(3 f t)(1 f t)=287 \mathrm{lbf}$
Thus (1.94) $\frac{\pi}{4}\left(\frac{3}{12} f t\right)^{2} V^{2}\left(\frac{21.5}{12} f t\right)=(287 l b f)\left(\frac{4}{12} f t\right)$, solve for $V_{j e t}=23.7 \frac{\mathbf{f t}}{\mathbf{s}}$ Ans.

P3.153 The 3-arm lawn sprinkler of Fig. P3. 153 receives $20^{\circ} \mathrm{C}$ water through the center at $2.7 \mathrm{~m}^{3} / \mathrm{hr}$. If collar friction is neglected, what is the steady rotation rate in $\mathrm{rev} / \mathrm{min}$ for (a) $\theta=0^{\circ}$; (b) $\theta=40^{\circ}$ ?


Solution: The velocity exiting each arm is

$$
\mathrm{V}_{\mathrm{o}}=\frac{\mathrm{Q} / 3}{(\pi / 4) \mathrm{d}^{2}}=\frac{2.7 /[(3600)(3)]}{(\pi / 4)(0.007)^{2}}=6.50 \frac{\mathrm{~m}}{\mathrm{~s}}
$$

With negligible air drag and bearing friction, the steady rotation rate (Example 3.15) is

$$
\omega_{\text {final }}=\frac{\mathrm{V}_{\mathrm{o}} \cos \theta}{\mathrm{R}} \text { (a) } \theta=0^{\circ}: \quad \omega=\frac{(6.50) \cos 0^{\circ}}{0.15 \mathrm{~m}}=43.3 \frac{\mathrm{rad}}{\mathrm{~s}}=414 \frac{\mathbf{r e v}}{\mathbf{m i n}} \quad \text { Ans. (a) }
$$

$$
\text { (b) } \theta=40^{\circ}: \quad \omega=\omega_{\mathrm{o}} \cos \theta=(414) \cos 40^{\circ}=\mathbf{3 1 7} \frac{\text { rev }}{\mathrm{min}} \quad \text { Ans. (b) }
$$

P3.154 Water at $20^{\circ} \mathrm{C}$ flows at $30 \mathrm{gal} / \mathrm{min}$ through the 0.75 -in-diameter double pipe bend of Fig. P3.154. The pressures are $p_{1}=30 \mathrm{lbf} / \mathrm{in}^{2}$ and $p_{2}=24 \mathrm{lbf} / \mathrm{in}^{2}$. Compute the torque $T$ at point $B$ necessary to keep the pipe from rotating.


Fig. P3.154
Solution: This is similar to Example 3.13, of the text. The volume flow $\mathrm{Q}=30 \mathrm{gal} / \mathrm{min}=$ $0.0668 \mathrm{ft}^{3} / \mathrm{s}$, and $\rho=1.94 \mathrm{slug} / \mathrm{ft}^{3}$. Thus the mass flow $\rho \mathrm{Q}=0.130$ slug $/ \mathrm{s}$. The velocity in the pipe is

$$
\mathrm{V}_{1}=\mathrm{V}_{2}=\mathrm{Q} / \mathrm{A}=\frac{0.0668}{(\pi / 4)(0.75 / 12)^{2}}=21.8 \frac{\mathrm{ft}}{\mathrm{~s}}
$$

If we take torques about point B, then the distance " $h_{1}$ " from p. 143, $=0$, and $h_{2}=3 \mathrm{ft}$. The final torque at point B, from "Ans. (a)" on p. 143 of the text, is
$\mathrm{T}_{\mathrm{B}}=\mathrm{h}_{2}\left(\mathrm{p}_{2} \mathrm{~A}_{2}+\dot{\mathrm{m}} \mathrm{V}_{2}\right)=(3 \mathrm{ft})\left[(24 \mathrm{psi}) \frac{\pi}{4}(0.75 \mathrm{in})^{2}+(0.130)(21.8)\right] \approx \mathbf{4 0} \mathbf{f t} \cdot \mathbf{l b f} \quad$ Ans.

P3.180 Water at $20^{\circ} \mathrm{C}$ is pumped at $1500 \mathrm{gal} / \mathrm{min}$ from the lower to the upper reservoir, as in Fig. P3.180. Pipe friction losses are approximated by $h f \approx 27 V^{2} /(2 g)$, where $V$ is the average velocity in the pipe. If the pump is 75 percent efficient, what horse-power is needed to drive it?


Solution: First evaluate the average velocity in the pipe and the friction head loss:

$$
\mathrm{Q}=\frac{1500}{448.8}=3.34 \frac{\mathrm{ft}^{3}}{\mathrm{~s}}, \quad \text { so } \quad \mathrm{V}=\frac{\mathrm{Q}}{\mathrm{~A}}=\frac{3.34}{\pi(3 / 12)^{2}}=17.0 \frac{\mathrm{ft}}{\mathrm{~s}} \quad \text { and } \quad \mathrm{h}_{\mathrm{f}}=27 \frac{(17.0)^{2}}{2(32.2)} \approx \mathbf{1 2 1} \mathbf{f t}
$$

Then apply the steady flow energy equation:

$$
\begin{gathered}
\frac{\mathrm{p}_{1}}{\rho \mathrm{~g}}+\frac{\mathrm{V}_{1}^{2}}{2 \mathrm{~g}}+\mathrm{z}_{1}=\frac{\mathrm{p}_{2}}{\rho \mathrm{~g}}+\frac{\mathrm{V}_{2}^{2}}{2 \mathrm{~g}}+\mathrm{z}_{2}+\mathrm{h}_{\mathrm{f}}-\mathrm{h}_{\mathrm{p}}, \\
\text { or: } 0+0+50=0+0+150+121-\mathrm{h}_{\mathrm{p}} \\
\text { Thus } \mathrm{h}_{\mathrm{p}}=221 \mathrm{ft}, \quad \text { so } \mathrm{P}_{\text {pump }}=\frac{\gamma \mathrm{Qh}_{\mathrm{p}}}{\eta}=\frac{(62.4)(3.34)(221)}{0.75} \\
=61600 \frac{\mathrm{ft} \cdot \mathrm{lbf}}{\mathrm{~s}} \approx \mathbf{1 1 2} \mathbf{~ h p} \text { Ans. }
\end{gathered}
$$

P3.183 The pump in Fig. P3. 183 creates a $20^{\circ} \mathrm{C}$ water jet oriented to travel a maximum horizontal distance. System friction head losses are 6.5 m . The jet may be approximated by the trajectory of friction-less particles. What power must be delivered by the pump?


Fig. P3. 183
Solution: For maximum travel, the jet must exit at $\theta=45^{\circ}$, and the exit velocity must be

$$
\mathrm{V}_{2} \sin \theta=\sqrt{2 \mathrm{~g} \Delta \mathrm{z}_{\max }} \quad \text { or: } \quad \mathrm{V}_{2}=\frac{[2(9.81)(25)]^{1 / 2}}{\sin 45^{\circ}} \approx 31.32 \frac{\mathrm{~m}}{\mathrm{~s}}
$$

The steady flow energy equation for the piping system may then be evaluated:

$$
\mathrm{p}_{1} / \gamma+\mathrm{V}_{1}^{2} / 2 \mathrm{~g}+\mathrm{z}_{1}=\mathrm{p}_{2} / \gamma+\mathrm{V}_{2}^{2} / 2 \mathrm{~g}+\mathrm{z}_{2}+\mathrm{h}_{\mathrm{f}}-\mathrm{h}_{\mathrm{p}}
$$

or: $0+0+15=0+(31.32)^{2} /[2(9.81)]+2+6.5-h_{\mathrm{p}}$, solve for $\mathrm{h}_{\mathrm{p}} \approx 43.5 \mathrm{~m}$
Then $\quad \mathrm{P}_{\text {pump }}=\gamma \mathrm{Qh}_{\mathrm{p}}=(9790)\left[\frac{\pi}{4}(0.05)^{2}(31.32)\right](43.5) \approx \mathbf{2 6 2 0 0} \mathbf{~ W}$ Ans.

