## Lecture 19 Transistor Amplifiers (II) Common-Emitter Amplifier

## **Outline**

- Common-source amplifier (summary)
- Common-emitter amplifier
- Common-emitter amplifier with current-source supply
- Common-emitter amplifier with emitter degeneration resistor

#### **Reading Assignment:**

Howe and Sodini; Chapter 8, Sections 8.4-8.6

#### **Announcement:**

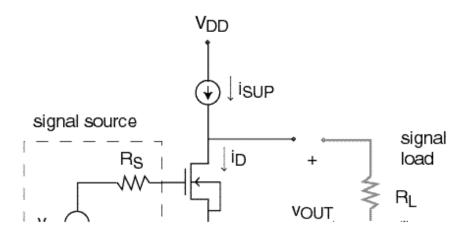
**Quiz #2:** Wednesday, November 15, 7:30-9:30 PM at Walker Memorial. Lectures #10 - #17. Calculator Required. Open book & notes.

**No Recitation on Wednesday:** Instructors will be available in their offices during recitation times

## **Summary of Key Concepts**

- Common-emitter amplifier with resistive supply
  - To maximize gain, large power supply required
  - High power consumption
- Performance improved by using common-emitter amplifier with current source supply.
- Two-port network computation of voltage gain, input resistance and output resistance of amplifier.

### **1. Common Source Amplifier:** with current source supply



Summary of small-signal results (unloaded):

- Voltage gain:  $A_{vo} = -g_m (r_o //r_{oc})$ .
- Input resistance  $:R_{in} =$
- Output resistance:  $R_{out} = r_o / / r_{oc}$ .

# **Relationship between circuit figures of merit and device parameters**

Remember:

$$g_{m} = \sqrt{2 I_{D} \frac{W}{L} \mu_{n} C_{ox}}$$
$$r_{o} = \frac{1}{n I_{D}} \frac{L}{I_{D}}$$

#### Then:

	Circuit Parameters		
Device*	$ A_{vo} $	R <sub>in</sub>	R <sub>out</sub>
Parameters	$g_{\rm m}(r_{\rm o}//r_{\rm oc})$		$r_{o}//r_{oc}$
I <sub>SUP</sub>		-	
W		_	-
$\mu_n C_{ox}$ `		_	-
L		-	

 $\ast$  adjustments are made to  $V_{GG}$  so that none of the other parameters change

CS amplifier with current source supply is a good voltage amplifier ( $R_{in}$  high and  $|A_{vo}|$  high), but  $R_{out}$  high too voltage gain degraded if  $R_L \ll r_o//r_{oc}$ .

## 2. Common-Emitter Amplifier:

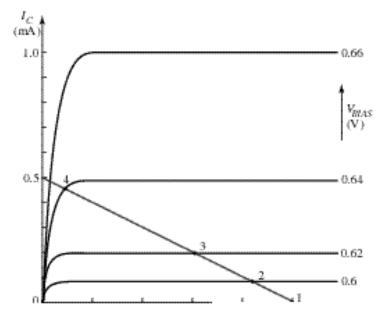
Circuit Topology:

Consider it first unloaded by R<sub>L</sub>. How does it work?

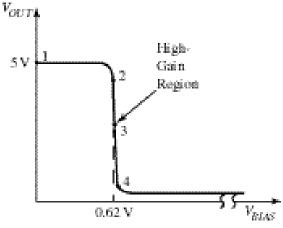
- $V_{BIAS}$ ,  $R_C$  and  $A_E$  of npn-BJT selected to bias transistor in forward active region (FAR) and obtain desired output bias point (i.e.  $V_{OUT} = 0$ ).
- $v_S$   $v_{BE}$   $i_B$   $i_C$   $v_{OUT}$ • A - v / v < 0: output out of phase from input b
- $A_v = v_{out} / v_s <0$ ; output out of phase from input, but if amplifier is well designed,  $|A_v|>1$ .

Watch notation:  $v_{OUT}(t) = V_{OUT} + v_{out}(t)$ 

#### **Load line of Common Emitter Amplifier:**

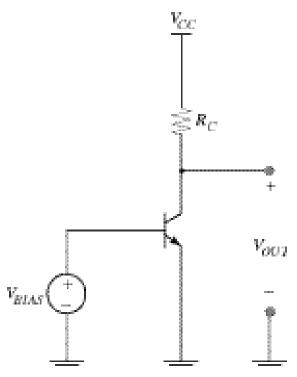


**Transfer characteristics of amplifier:** 



- Graphical approach
  - Plot I<sub>C</sub> as a function of the DC base-emitter voltage V<sub>BIAS</sub>
  - Note that normally we plot  $I_C$  vs.  $I_B$ , so we have to return to Ebers-Moll equations
- We can plot the forward active current for
  - $V_{CE} = V_{OUT} > V_{CE(sat)}$
  - Note that the range of  $V_{BIAS}$  is only 600-660 mV

## **Biasing the CE Amplifier**



The collector current is given by the Ebers-Moll Equation:

$$\mathbf{I}_{\mathbf{C}} = \mathbf{I}_{\mathbf{S}} \exp \frac{\mathbf{V}_{\mathbf{BE}}}{\mathbf{V}_{\mathbf{th}}} - 1 - \frac{\mathbf{I}_{\mathbf{S}}}{\mathbf{R}} \exp \frac{\mathbf{V}_{\mathbf{BC}}}{\mathbf{V}_{\mathbf{th}}} - 1$$

In Forward Active Region

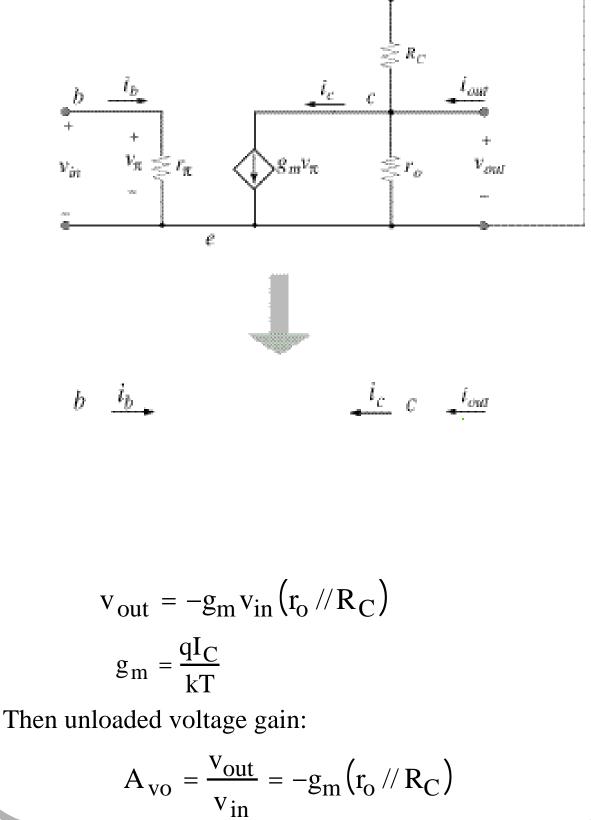
$$\mathbf{I}_{\mathbf{C}} \quad \mathbf{I}_{\mathbf{S}} \cdot \exp \frac{\mathbf{V}_{\mathbf{B}\mathbf{E}}}{\mathbf{V}_{\mathbf{t}\mathbf{h}}} = \mathbf{I}_{\mathbf{S}} \cdot \exp \frac{\mathbf{V}_{\mathbf{B}\mathbf{I}\mathbf{A}\mathbf{S}}}{\mathbf{V}_{\mathbf{t}\mathbf{h}}}$$

Output Voltage

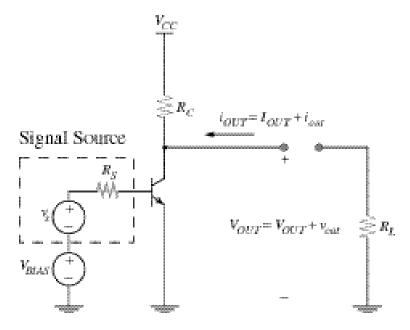
$$V_{OUT} = V_{CE} = V_{CC} - I_C R_C$$

Typically select  $V_{OUT} = 1 / 2 V_{CC}$ 

**Small-signal voltage gain:** draw small-signal equivalent circuit model.



#### **Signal Swing and Effect of input/output loading:**



• Upswing limited by resistive divider:

$$v_{OUT,max} = V_{CC} \frac{R_L}{R_L + R_C}$$

- Downswing not affected by loading  $V_{OUT,min} = V_{CE,sat}$
- Voltage swing

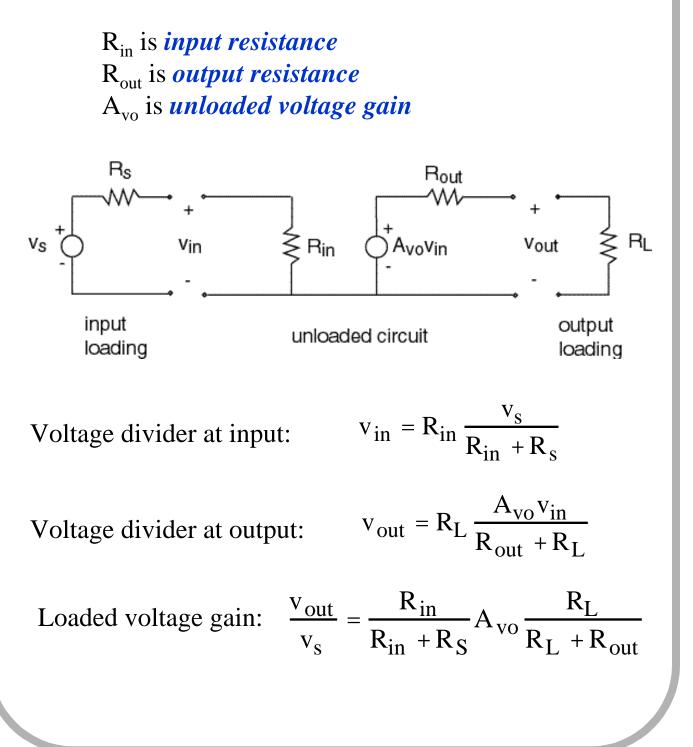
$$\mathbf{v}_{\text{OUT}} = \mathbf{v}_{\text{out}} = \mathbf{V}_{\text{CC}} \frac{\mathbf{R}_{\text{L}}}{\mathbf{R}_{\text{L}} + \mathbf{R}_{\text{C}}} - \mathbf{V}_{\text{CE, sat}}$$

- Voltage gain:
  - Input loading  $(R_s)$ :  $R_s$  reduces voltage gain because it forms a resistor divider with r;
  - Output loading (R<sub>L</sub>): R<sub>L</sub> reduces voltage gain because it draws current.

$$|A_v| = \frac{r}{r + R_S} g_m (r_o / / R_C / / R_L) < g_m (r_o / / R_C)$$

#### **Effect of loading on small-signal operation**

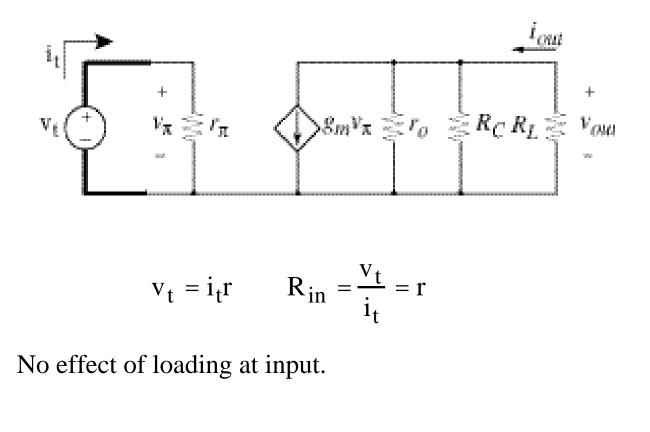
Two-port network view of small-signal equivalent circuit model of amplifier:



## **Input Resistance**

- Calculation of input resistance, R<sub>in</sub>:
  - Load amplifier with  $R_L$
  - Apply test voltage (or current) at input, measure test current (or voltage).

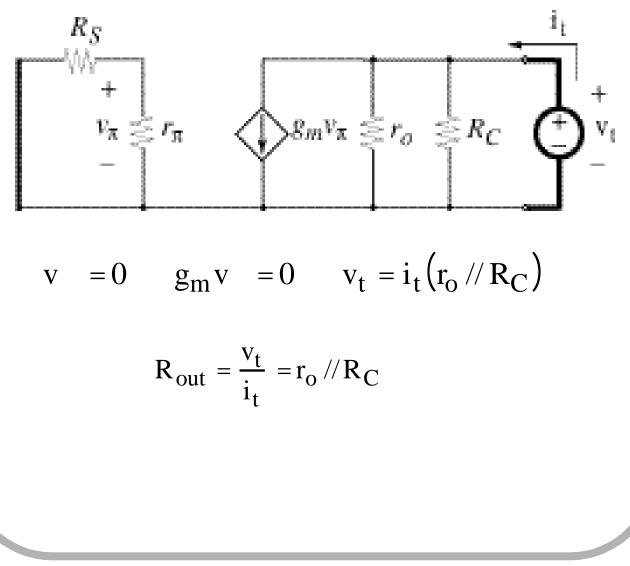
For common-emitter amplifier:



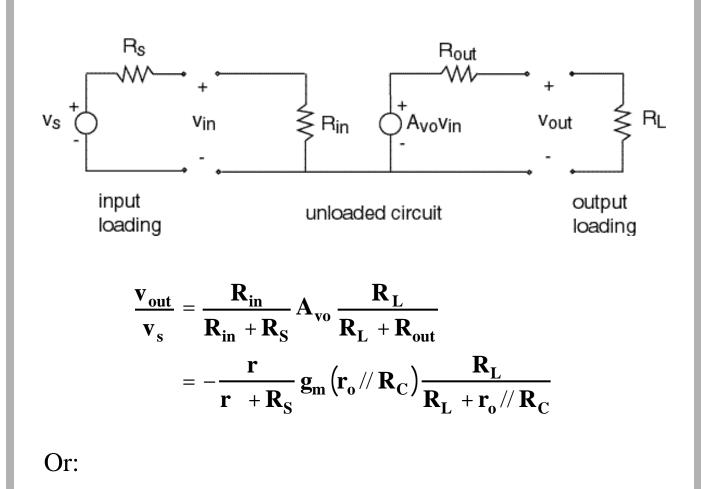
## **Output Resistance**

- Calculation of input resistance, R<sub>out</sub>:
  - Load amplifier with R<sub>s</sub>
  - Apply test voltage (or current) at output, measure test current (or voltage).

For common-emitter amplifier:



#### **Two-port network view of common-source amplifier**



$$\frac{\mathbf{v}_{out}}{\mathbf{v}_{s}} = -\frac{\mathbf{r}}{\mathbf{r} + \mathbf{R}_{s}} \mathbf{g}_{m} \left( \mathbf{r}_{o} / / \mathbf{R}_{C} / / \mathbf{R}_{L} \right)$$
$$\mathbf{R}_{out} = \mathbf{r}_{o} / / \mathbf{R}_{C}$$
$$\mathbf{R}_{in} = \mathbf{r}$$

#### Design issues of common-emitter amplifier (unloaded)

• To maximize the output swing, set  $V_{OUT} = V_{CC}/2$ . The load resistor value is coupled with the collector current through the load line equation

$$I_{C} = \frac{V_{CC} - V_{OUT}}{R_{C}} \quad \frac{V_{CC}}{2R_{C}}$$

• The transconductance is therefore

$$g_{m} = \frac{I_{C}}{V_{th}} = \frac{V_{CC}}{2R_{C}V_{th}}$$

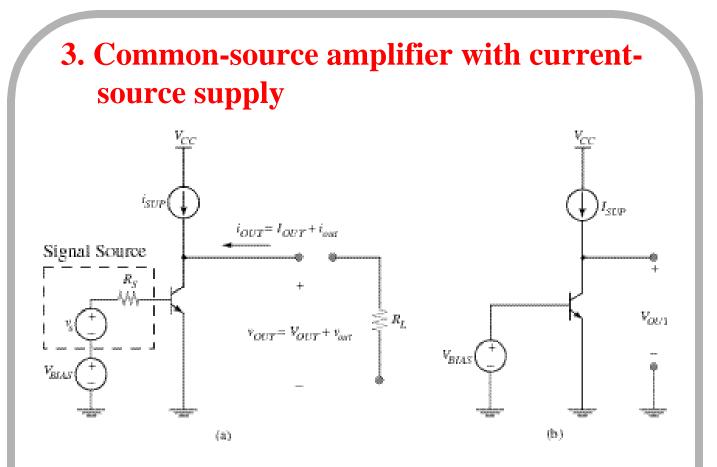
• The small signal gain voltage gain (for  $r_0 >> R_C$ )

$$A_{v} \quad g_{m}R_{C} = \frac{-V_{CC}}{2 V_{h}}$$

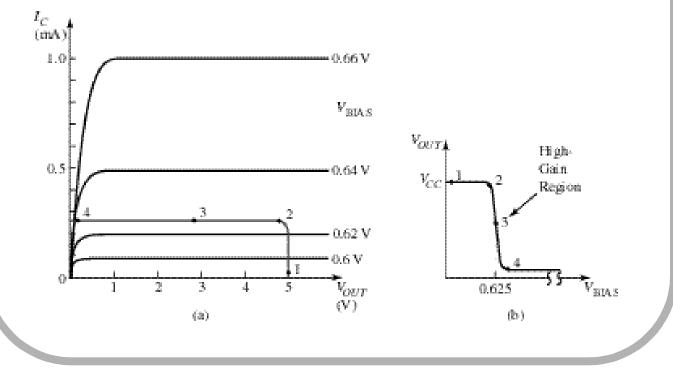
#### **Issue:**

• To increase the voltage gain, the only option is to increase the supply voltage which wastes power

**Solution:** CE amplifier with current source supply



#### CE Amplifier with Idealized Current Source Loadline :



# Small-Signal Model for CE Amplifier with Current Source Supply $\begin{array}{c} \downarrow \\ \psi_{in} \\ + \\ \psi_{\pi} \\ = \\ r_{\pi} \\ - \\ e \end{array}$

• Voltage Gain (unloaded)

$$\mathbf{A}_{vo} = \frac{\mathbf{v}_{out}}{\mathbf{v}_{in}} = -\mathbf{g}_{m} (\mathbf{r}_{o} / / \mathbf{r}_{oc})$$

• For a well designed current source,  $r_{oc} >> r_{o}$ , hence common emitter amplifier gain reduces to:

$$\mathbf{A_{vo}} \quad \mathbf{g_m}\mathbf{r_o} = - \frac{\mathbf{I_C}}{\mathbf{V_{th}}} \quad \frac{\mathbf{V_A}}{\mathbf{I_C}} = -\frac{\mathbf{V_A}}{\mathbf{V_{th}}}$$

- Final expression depends on device dimensions and parameters
  - (e.g., base width and the ratio of base doping to collector doping)

## **Relationship between common emitter amplifier circuit figures of merit and device parameters**

Remember:

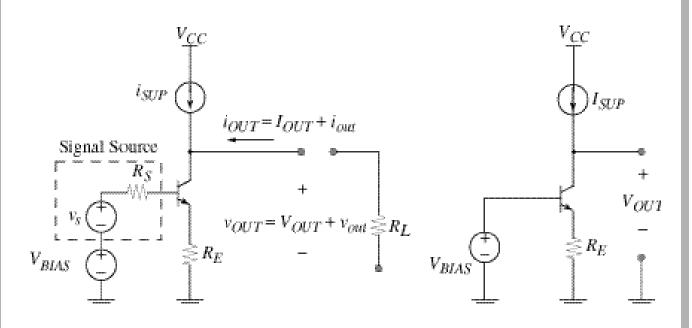
$$g_{\rm m} = \frac{I_{\rm C}}{V_{\rm th}}$$
$$r_{\rm o} \quad \frac{V_{\rm A}}{I_{\rm C}}$$

Then:

	Circuit Parameters			
Device Parameters	$ A_{vo} $	R <sub>in</sub>	R <sub>out</sub>	
	$g_{\rm m}(r_{\rm o}//r_{\rm oc})$	r	$r_{o}//r_{oc}$	
I <sub>SUP</sub>	-			
0	-		-	
V <sub>A</sub>		-		

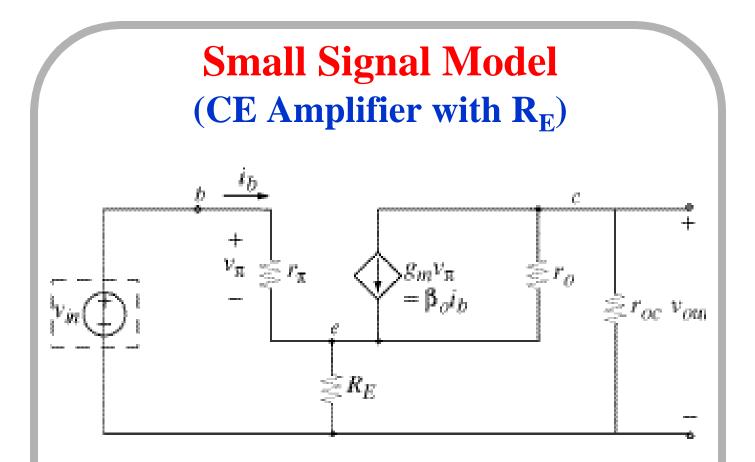
CE amplifier with current source supply is a good voltage amplifier ( $R_{in}$  medium and  $|A_{vo}|$  high), but  $R_{out}$  high too voltage gain degraded if  $R_L \ll r_o//r_{oc}$ .

## **Common Emitter Amplifier** (with emitter degeneration resistor)



- Addition of emitter resistance leads to increase in input and output resistance
- Voltage gain depends predominantly on the emitter resistance resulting in a well controlled gain
  - Gain relatively independent of temperature and process variations

$$\mathbf{V}_{BIAS} = \mathbf{V}_{BE} + \frac{\left(\mathbf{F} + 1\right)\mathbf{I}_{C}}{\mathbf{F}}\mathbf{R}_{E} \quad \mathbf{V}_{BE} + \mathbf{I}_{C}\mathbf{R}_{E}$$
$$\mathbf{V}_{BE} = \mathbf{V}_{th} \ln \frac{\mathbf{I}_{C}}{\mathbf{I}_{S}}$$
$$\mathbf{I}_{C} = \mathbf{I}_{SUP}$$



- Addition of emitter resistance leads to increase in input and output resistance by a factor  $(1 + g_m R_E)$
- Voltage gain reduced by a factor  $(1 + g_m R_E)$

$$A_{v} - \frac{g_{m} [r_{oc} // r_{o} (1 + g_{m} R_{E})]}{1 + g_{m} R_{E}} - \frac{g_{m} r_{oc}}{1 + g_{m} R_{E}}$$
$$R_{in} = r (1 + g_{m} R_{E})$$
$$R_{out} - r_{oc} // r_{o} (1 + g_{m} R_{E})$$

## What did we learn today? Summary of Key Concepts

- Common-emitter amplifier with resistive supply
  - To maximize gain, large power supply required
  - High power consumption
- Performance improved by using common-emitter amplifier with current source supply.
- Two-port network computation of voltage gain, input resistance and output resistance of amplifier.