

SHORT CIRCUIT FAULT CALCULATIONS

Short circuit fault calculations as required to be performed on all electrical service entrances by National Electrical Code 110-9, 110-10. These calculations are made to assure that the service equipment will clear a fault in case of short circuit.

To perform the fault calculations the following information must be obtained:

1. Available Power Company Short circuit KVA at transformer primary : Contact Power Company, may also be given in terms of $R + jX$.
2. Length of service drop from transformer to building, Type and size of conductor, ie., 250 MCM, aluminum.
3. Impedance of transformer, KVA size.
 - A. %R = Percent Resistance
 - B. %X = Percent Reactance
 - C. %Z = Percent Impedance
 - D. KVA = Kilovoltamp size of transformer. (Obtain for each transformer if in Bank of 2 or 3)
4. If service entrance consists of several different sizes of conductors, each must be adjusted by (Ohms for 1 conductor)
(Number of conductors)

This must be done for R and X

Three Phase Systems

Wye Systems: 120/208V 3 \emptyset , 4 wire
277/480V 3 \emptyset 4 wire

Delta Systems: 120/240V 3 \emptyset , 4 wire
240V 3 \emptyset , 3 wire
480 V 3 \emptyset , 3 wire

Single Phase Systems:

Voltage 120/240V 1 \emptyset , 3 wire. Separate line to line and line to neutral calculations must be done for single phase systems. Voltage in equations (KV) is the secondary transformer voltage, line to line.

Base KVA is 10,000 in all examples.

Only those components actually in the system have to be included, each component must have an X and an R value. Neutral size is assumed to be the same size as the phase conductors.

See page 14 & 27 for example in Buss Book.

Short Circuit Calculations

Only one calculation needs to be done for most 3 phase systems. This is for the per unit method.

3 Phase

$$I_{SCA} = \frac{KVA \text{ Base}}{\sqrt{3} \text{ KVLL total PUZ}}$$

$$KVA \text{ Base} = 10,000$$

Single Phase

Two separate calculations must be done for single phase systems.

$$I_{SCA} = \frac{KVA \text{ Base}}{(KV \text{ line to line}) (total PUZ)}$$

$$I_{SCA} = \frac{KVA \text{ Base}}{(KV \text{ line to neutral}) (total PUZ)}$$

$$KVA \text{ Base} = 10,000$$

$$KVLL \quad .230KV$$

$$KVLL \quad .115KV$$

See page 12 Buss Book for transformer and wire equations.

Table 1- Transformer Impedance Data

Percent R, X and Z based on Transformer KVA

| Transformer Rating KVA | X/R | R % | X % | Z % |
|------------------------|------|-------|-------|------|
| 150 | 3.24 | 1.23 | 4.0 | 4.19 |
| 225 | 3.35 | 1.19 | 4.0 | 4.17 |
| 300 | 3.50 | 1.14 | 4.0 | 4.16 |
| 500 | 3.85 | 1.04 | 4.0 | 4.12 |
| 750 | 5.45 | 0.94 | 5.1 | 5.19 |
| 1000 | 5.70 | 0.89 | 5.1 | 5.19 |
| 1500 | 6.15 | 0.83 | 5.1 | 5.18 |
| 2000 | 6.63 | 0.77 | 5.1 | 5.17 |
| 150 | 1.5 | 1.111 | 1.665 | 2.0 |
| 225 | 1.5 | 1.111 | 1.665 | 2.0 |
| 300 | 1.5 | 1.111 | 1.665 | 2.0 |
| 500 | 1.5 | 1.111 | 1.665 | 2.0 |

Note 1: These values are for three phase, liquid filled, self-cooled transformers.

Note 2: Due to the trend toward lower impedance transformers for better voltage regulation, the actual transformer impedances may deviate from the NEMA Standard given at left. Therefore, for actual values, obtain nameplate impedance from owner or manufacturer. The percent X and percent R values are desirable for calculation.

Table 12—Distribution Transformers—Three-phase Padmount—Single-voltage Primary Maximum Line-to-Line Primary Voltage—25 kV WYE—18 kV Delta

| kVA | LOW VOLTAGE | | | | | |
|--------|-------------|------|------|----------|------|------|
| | 208Y/120 | | | 480Y/277 | | |
| | % IZ* | % IR | % IX | % IZ* | % IR | % IX |
| 75 | 1.55 | 1.27 | 0.89 | 1.60 | 1.29 | 0.94 |
| 75A | 2.68 | 1.34 | 2.32 | 2.87 | 1.37 | 2.52 |
| 112.5 | 1.60 | 1.10 | 1.16 | 1.60 | 1.11 | 1.16 |
| 112.5A | 3.54 | 1.10 | 3.36 | 3.56 | 1.11 | 3.38 |
| 150 | 1.95 | 1.08 | 1.63 | 1.90 | 1.11 | 1.55 |
| 150A | 4.63 | 1.08 | 4.50 | 4.62 | 1.11 | 4.48 |
| 225 | 2.00 | 1.05 | 1.70 | 2.00 | 1.01 | 1.73 |
| 225A | 4.66 | 1.09 | 4.53 | 4.74 | 1.06 | 4.62 |
| 300 | 2.05 | 0.95 | 1.82 | 2.15 | 0.88 | 1.96 |

| kVA | LOW VOLTAGE | | | | | |
|------|-------------|-------|-------|----------|------|------|
| | 208Y/120 | | | 480Y/277 | | |
| | % IZ* | % IR | % IX | % IZ* | % IR | % IX |
| 300A | 5.23 | 0.95 | 5.14 | 4.93 | 0.88 | 4.85 |
| 500 | 2.00 | 0.88 | 1.80 | 2.10 | 0.85 | 1.92 |
| 500A | 5.56 | 0.89 | 5.49 | 5.33 | 0.85 | 5.26 |
| 750 | 5.75 | 0.93 | 5.68 | 5.75 | 0.88 | 5.68 |
| 1000 | 5.75 | 0.92 | 5.68 | 5.75 | 0.85 | 5.69 |
| 1500 | | | | 5.75 | 0.72 | 5.70 |
| 2000 | | | | 5.75 | 0.68 | 5.71 |
| 2500 | | | | 5.75 | 0.61 | 5.72 |

*% IZ typical only through 500 kVA.

▲Optional impedance values—not standard.

3-phase pads COMPAD III maximum coil voltage of 18,000 volts.

TYPICAL PERFORMANCE DATA - GENERAL PURPOSE-1966 DESIGNS,
1.2 KV CLASS, 60 HZ, 40°C AMBIENT

| KVA & Phase | Core Loss (Watts) | Coil Loss (Watts) | | Full Load Losses (Watts) | Impedance | | | Percent Efficiency | | | | % Voltage Regulation | | Avg Wind. Temp Rise ° C | Max Case Surface Temp ° C | Max KVA in 50°C Amb. | |
|---|-------------------|-------------------|------------------|--------------------------|-----------|------|------|--------------------|----------|----------|----------|----------------------|------------|-------------------------|---------------------------|----------------------|--|
| | | @ 25°C | @ STD Base Temp. | | % R | % X | % Z | Full Load | 3/4 Load | 1/2 Load | 1/4 Load | .8 P.F. | Unity P.F. | | | | |
| PL-21B (All values given are at 135°C except coil loss which is also given at 25°C) | | | | | | | | | | | | | | | | | |
| 5-1Ø | 44 | 103 | 147 | 191 | 2.94 | 1.68 | 3.4 | 96.3 | 96.75 | 96.8 | 95.9 | 3.4 | 2.95 | 102 | 52.9 | | |
| 7-1/2-1Ø | 56 | 127 | 181 | 237 | 2.42 | 1.84 | 3.04 | 96.95 | 97.25 | 97.35 | 96.5 | 3.1 | 2.45 | 100 | 55.2 | | |
| 10-1Ø | 68 | 142 | 204 | 272 | 2.04 | 1.92 | 2.75 | 97.35 | 97.6 | 97.65 | 96.8 | 2.8 | 2.05 | 112 | 62.5 | | |
| 15-1Ø | 95 | 167 | 239 | 334 | 1.60 | 2.02 | 2.58 | 97.8 | 98.0 | 98.0 | 97.2 | 2.5 | 1.65 | 104 | 58.3 | | |
| 25-1Ø | 160 | 246 | 352 | 512 | 1.41 | 2.29 | 2.7 | 98.0 | 98.1 | 98.0 | 97.1 | 2.5 | 1.48 | 109 | 63.7 | | |
| PL-23A (All values given are at 170°C except coil loss which is also given at 25°C) | | | | | | | | | | | | | | | | | |
| 37-1/2-1Ø | 160 | 900 | 1405 | 1565 | 3.75 | 2.88 | 4.7 | 95.9 | 96.7 | 97.3 | 97.4 | 4.7 | 3.8 | | 45 | 36 | |
| 50-1Ø | 208 | 1040 | 1625 | 1833 | 3.25 | 3.0 | 4.4 | 96.4 | 97.0 | 97.6 | 97.5 | 4.4 | 3.3 | | 48 | 50 | |
| 75-1Ø | 218 | 1170 | 1825 | 2043 | 2.44 | 3.65 | 4.4 | 97.3 | 97.8 | 98.2 | 98.2 | 4.2 | 2.5 | | | 75 | |
| 100-1Ø | 320 | 1425 | 2230 | 2550 | 2.24 | 3.44 | 4.1 | 97.5 | 97.9 | 98.2 | 98.1 | 3.9 | 2.3 | | 41 | 100 | |
| 167-1Ø | 520 | 1660 | 2590 | 3110 | 1.55 | 3.33 | 3.7 | 98.1 | 98.4 | 98.6 | 98.3 | 3.3 | 1.6 | | 34 | 167 | |
| PL-21A (All values given are at 135°C except coil loss which is also given at 25°C) | | | | | | | | | | | | | | | | | |
| 3-3Ø | 45 | 79 | 113 | 158 | 3.76 | 1.0 | 3.9 | 95.0 | 95.1 | 95.3 | 93.5 | 3.6 | 3.75 | 114 | 62 | | |
| 6-3Ø | 83 | 114 | 163 | 246 | 2.72 | 1.72 | 3.2 | 96.1 | 96.3 | 96.0 | 94.2 | 3.2 | 2.74 | 112 | 62 | | |
| 9-3Ø | 120 | 120 | 172 | 292 | 2.31 | 1.16 | 2.6 | 96.9 | 96.9 | 96.5 | 94.6 | 2.6 | 2.32 | 112 | 64 | | |
| 15-3Ø | 140 | 220 | 315 | 455 | 2.10 | 1.82 | 2.8 | 97.1 | 97.3 | 97.2 | 96.0 | 2.7 | 2.14 | 110 | 65 | | |
| PL-23A (All values given are at 170°C except coil loss which is also given at 25°C) | | | | | | | | | | | | | | | | | |
| 30-3Ø | 268 | 720 | 1125 | 1393 | 3.75 | 2.04 | 4.3 | 95.5 | 96.1 | 96.4 | 95.6 | 4.2 | 3.8 | | 35 | 30 | |
| 45-3Ø | 360 | 785 | 1225 | 1585 | 2.73 | 1.97 | 3.4 | 96.5 | 96.9 | 97.1 | 96.2 | 3.4 | 2.8 | | 35.2 | 45 | |
| 75-3Ø | 510 | 1160 | 1815 | 2325 | 2.42 | 2.1 | 3.2 | 97.0 | 97.3 | 97.4 | 96.7 | 3.2 | 2.5 | | 41.5 | 75 | |
| 112.5-3Ø | 415 | 1850 | 2890 | 3305 | 2.56 | 3.69 | 4.5 | 97.1 | 97.6 | 98.0 | 97.9 | 4.3 | 2.7 | | 46 | 109 | |
| 150-3Ø | 580 | 1860 | 2910 | 3490 | 1.94 | 4.07 | 4.5 | 97.7 | 98.0 | 98.2 | 98.0 | 4.0 | 2.1 | | 38 | 150 | |
| 225-3Ø | 770 | 2800 | 4370 | 5140 | 1.95 | 4.8 | 5.2 | 97.7 | 98.1 | 98.3 | 98.1 | 4.5 | 2.1 | | 54.5 | 217 | |
| 300-3Ø | 1200 | 3260 | 5090 | 6290 | 1.7 | 4.96 | 5.3 | 97.9 | 98.2 | 98.3 | 98.0 | 4.4 | 1.8 | | 55 | 295 | |
| 500-3Ø | 1900 | 4500 | 7030 | 8930 | 1.4 | 5.11 | 5.3 | 98.2 | 98.4 | 98.5 | 98.1 | 4.3 | 1.6 | | 52 | 483 | |

Appendix

Table 5—Estimated Secondary Short-circuit Currents For Single-phase, Three-wire Secondary Distribution Transformers

(7200/12,470Y—120/240-VOLT TRANSFORMER)

MAXIMUM SYMMETRICAL SHORT-CIRCUIT CURRENT FOR STANDARD 120/240-VOLT, 3 WIRE, SINGLE-PHASE DISTRIBUTION TRANSFORMER (LINE-TO-NEUTRAL FAULT AT TRANSFORMER TERMINALS)

| Available Primary 3-phase Short-circuit MVA | Transformer kVA Rating, Single Phase | | | | | |
|--|---|--------|--------|--------|--------|--------|
| | 25 | 37.5 | 50 | 75 | 100 | 167 |
| | Normal-load Continuous Current—Amperes at 240 Volts | | | | | |
| | 104 | 156 | 208 | 313 | 417 | 696 |
| Short-circuit Symmetrical Current at 120 Volts | | | | | | |
| 25 | 7,600 | 13,300 | 16,500 | 22,100 | 29,800 | 42,400 |
| 50 | 7,800 | 14,000 | 17,600 | 24,300 | 34,000 | 51,900 |
| 100 | 7,950 | 14,400 | 18,200 | 25,600 | 36,500 | 58,100 |
| 150 | 8,000 | 14,500 | 18,400 | 26,100 | 37,400 | 60,500 |
| 250 | 8,000 | 14,600 | 18,600 | 26,400 | 38,200 | 62,500 |
| 500 | 8,100 | 14,700 | 18,700 | 26,700 | 38,700 | 64,000 |
| 750 | 8,100 | 14,700 | 18,800 | 26,800 | 38,900 | 64,500 |
| Unlimited | 8,100 | 14,800 | 18,850 | 27,000 | 39,300 | 65,600 |

| TRANSFORMER FULL-WINDING IMPEDANCE ON RATED kVA, (7200/12,470Y—120/240-VOLT TRANSFORMER) | | | | | | |
|--|-----|-----|-----|-----|-----|-----|
| % IR | 1.2 | 1.0 | 1.0 | 0.9 | 0.9 | 0.9 |
| % IX | 1.6 | 1.3 | 1.4 | 1.6 | 1.4 | 1.4 |

Table 6—Estimated Secondary Short-circuit Currents for GE Three-phase Padmount Distribution Transformers Single-voltage Primary.

LINE-TO-LINE PRIMARY VOLTAGE 25 kV WYE—18 kV DELTA

| Available Primary 3-phase Short-circuit MVA | Secondary Voltage Rating | Transformer kVA Rating | | | | | | |
|---|--------------------------|------------------------|-------------------------|--------|--------|--------|--------|--------|
| | | 75 | 112.5 | 150 | 225 | 300 | 500 | |
| | | | Transformer Impedance—% | | | | | |
| | (1) 480Y/277V | %IR | 1.29 | 1.11 | 1.11 | 1.01 | 0.89 | 0.85 |
| | %IX | 0.94 | 1.16 | 1.55 | 1.73 | 1.96 | 1.92 | |
| | (2) 208Y/120V | %IR | 1.27 | 1.10 | 1.08 | 1.05 | 1.05 | 0.89 |
| | | %IX | 0.90 | 1.16 | 1.63 | 1.70 | 1.82 | 1.80 |
| Maximum Short-circuit Symmetrical rms Amperes | | | | | | | | |
| 100 | (1) | | 5,500 | 8,050 | 8,900 | 12,300 | 14,900 | 23,500 |
| | (2) | | 13,000 | 18,575 | 20,000 | 28,500 | 35,200 | 56,300 |
| 250 | (1) | | 5,600 | 8,300 | 9,250 | 13,000 | 16,000 | 26,400 |
| | (2) | | 13,225 | 19,150 | 20,800 | 30,100 | 37,800 | 63,400 |
| 500 | (1) | | 5,625 | 8,400 | 9,375 | 13,300 | 16,400 | 27,500 |
| | (2) | | 13,300 | 19,350 | 21,000 | 30,700 | 38,700 | 66,200 |



Avail. primary 3-phase short-circuit = 250 MVA
13.2 kV—208y/120V
225 kVA % Z = 2.2

Secondary 3φ bolted fault

Solve for the Secondary Fault using the per-unit method.

Select 225 kVA as the study base

$$X \text{ Utility Source} = \frac{225 \text{ kVA}}{250,000 \text{ kVA}} = 0.0009 \text{ pu}$$

$$X \text{ Trans} = (.017) \left(\frac{225 \text{ kVA}}{225 \text{ kVA}} \right) = 0.017 \text{ pu}$$

$$X = X \text{ trans} + X \text{ utility} = 0.0179$$

$$R \text{ trans} = (0.0105) \left(\frac{225 \text{ kVA}}{225 \text{ kVA}} \right) = 0.0105 \text{ pu}$$

$$Z = \sqrt{R^2 + X^2} = \sqrt{(0.0105)^2 + (0.0179)^2} = 0.0208$$

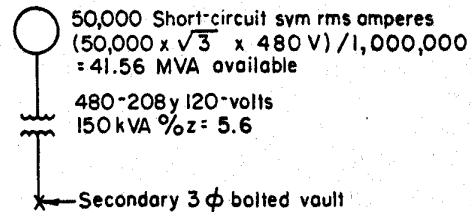
$$I_{sc} = \frac{kVA_b}{\sqrt{3} (KV) (Z \text{ pu})} = \frac{225}{\sqrt{3} (.208) (.0208)} = 30,095 \text{ 3}\phi \text{ Short-circuit Symmetrical rms Amperes at Transformer Terminals}$$

Appendix

Table 7—Estimated Secondary Short-circuit Currents For GE Type “QHT” Dry-type 3-phase Transformers

PRIMARY RATING 600 VOLTS AND BELOW, SECONDARY RATING 480Y/277V and 208/120V

| Available Short-circuit Symmetrical rms Amperes | Transformer kVA Rating | | | | | | | | | | | |
|---|------------------------|------|------|-------|-------|-------|-------|-------|-------|--------|--------|--------|
| | | 6 | 9 | 15 | 30 | 45 | 75 | 112.5 | 150 | 225 | 300 | 500 |
| | Transformer Impedance | | | | | | | | | | | |
| | % IR | 2.72 | 2.31 | 2.1 | 3.8 | 2.52 | 2.27 | 2.43 | 2.35 | 1.15 | 1.8 | 1.6 |
| | % IX | 1.72 | 1.16 | 1.80 | 1.37 | 1.73 | 1.91 | 3.87 | 5.0 | 5.5 | 4.5 | 5.9 |
| Short-circuit Symmetrical rms Amperes | | | | | | | | | | | | |
| Secondary Voltage | 480 | 225 | 415 | 640 | 885 | 1,700 | 2,810 | 2,690 | 2,925 | 4,050 | 5,800 | 7,100 |
| | 208 | 515 | 960 | 1,475 | 2,035 | 3,925 | 6,500 | 6,200 | 6,750 | 9,350 | 13,400 | 16,400 |
| 50,000 | 480 | 225 | 420 | 645 | 890 | 1,740 | 2,925 | 2,820 | 3,085 | 4,400 | 6,550 | 8,260 |
| | 208 | 520 | 965 | 1,485 | 2,050 | 4,005 | 6,750 | 6,500 | 7,125 | 10,151 | 15,100 | 19,160 |
| 200,000 | 480 | 226 | 420 | 650 | 845 | 1,760 | 3,010 | 2,925 | 3,450 | 4,700 | 7,200 | 9,400 |
| | 208 | 520 | 970 | 1,495 | 2,060 | 4,065 | 7,010 | 6,750 | 7,450 | 10,860 | 16,600 | 21,700 |



Solve for the Secondary Fault using the per-unit method.

Select 150 kVA as the study base.

$$X_{\text{available}} = \frac{150 \text{ kVA}}{41,570 \text{ kVA}} = 0.0036 \text{ pu}$$

$$X_{\text{trans}} = (.050) \frac{150 \text{ kVA}}{150 \text{ kVA}} = 0.050 \text{ pu}$$

$$X = X_{\text{avail.}} + X_{\text{trans}} = 0.0036 + .050 = .0536 \text{ pu}$$

$$R_{\text{trans}} = (.0235) \left(\frac{150 \text{ kVA}}{150 \text{ kVA}} \right) = 0.0235 \text{ pu}$$

$$Z = \sqrt{R^2 + X^2} = \sqrt{(0.0235)^2 + (0.0536)^2} = 0.0585$$

$$I_{\text{sc}} = \frac{\text{kVA}_b}{\sqrt{3} (\text{kV}) (Z)} = \frac{150}{\sqrt{3} (.208) (.0585)}$$

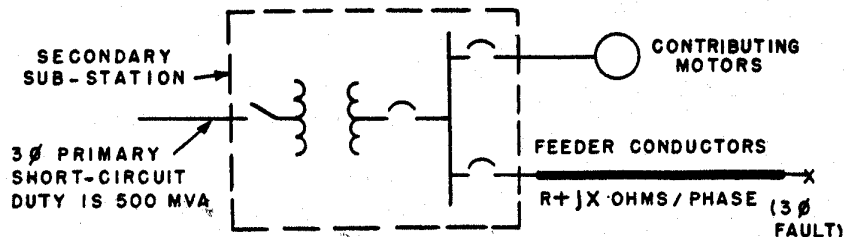
$$I_{\text{sc}} = 7,117 \text{ 3}\phi \text{ Short-circuit Sym. rms Amperes at transformer terminals}$$

Estimated Short-circuit Current at the End of Low-voltage Feeder (See Figs. 25-1—25-30)

Power-system maximum estimated short-circuit currents, as functions of distance along feeder conductors fed from standard three-phase radial secondary unit substations, can be read directly in rms symmetrical amperes from a series of curves, Fig. 25-1 through 25-30. The one-line diagram shows the typical radial circuit investigated.

The conditions on which the curves are based were as follows:

1. The fault was a bolted three-phase short circuit.
2. The primary three-phase short-circuit duty was 500 MVA (60 cycles) for all curves. A typical supply-system X/R at the low-voltage bus was used in calculating the curves for each case.
3. Motor contributions through the bus to the point of short circuit were included in the



Typical circuit investigated to show effect on short-circuit duty as point of fault is moved away from the low-voltage bus along the feeder conductors

calculations on the basis of 100 percent contribution for the 240-, 480-, and 600-volt systems and 50 percent contribution for the 208-volt systems.

4. The feeder-conductor impedance values used in the calculations are indicated for various conductor sizes.

These curves can also be used to select feeder conductor sizes and lengths needed to reduce short-circuit duties to desired smaller values. Note that conductors thus selected must be further checked to assure adequate load and short-circuit capabilities and acceptable voltage drop.

Appendix

Table 11—Distribution Transformers—Single-phase

| kVA | Low Voltage | %IR | %IX | %IZ | kVA | Low Voltage | %IR | %IX | %IZ |
|--------------------------------|--------------|-----|-----|-----|--|--------------|-----|-----|-----|
| HIGH VOLTAGE 2400/4160Y | | | | | HIGH VOLTAGE 7200/12470Y OR 12470GRDY/7200 | | | | |
| 5 | 120/240 | 2.0 | 1.5 | 2.5 | 5 | 120/240 | 2.2 | 2.2 | 3.1 |
| 10 | | 1.2 | 0.7 | 1.4 | 10 | | 1.4 | 0.8 | 1.6 |
| 15 | | 1.2 | 1.1 | 1.6 | 15 | | 1.3 | 1.2 | 1.8 |
| 25 | | 1.1 | 1.4 | 1.8 | 25 | | 1.2 | 1.6 | 2.0 |
| 37½ | | 0.9 | 1.2 | 1.5 | 37½ | | 1.0 | 1.3 | 1.6 |
| 50 | | 0.9 | 1.3 | 1.6 | 50 | | 1.0 | 1.4 | 1.7 |
| 75 | 0.9 | 1.3 | 1.6 | 75 | 0.9 | 1.6 | 1.8 | | |
| 100 | 0.9 | 1.6 | 1.8 | 100 | 0.9 | 1.4 | 1.7 | | |
| 167 | 0.9 | 1.6 | 1.8 | 167 | 0.9 | 1.4 | 1.7 | | |
| 10 | 240/480 | 1.1 | 1.0 | 1.5 | 10 | 240/480 | 1.4 | 0.8 | 1.6 |
| 15 | | 1.1 | 1.0 | 1.5 | 15 | | 1.3 | 0.9 | 1.6 |
| 25 | | 1.1 | 1.5 | 1.9 | 25 | | 1.2 | 1.6 | 2.0 |
| 37½ | | 0.9 | 1.3 | 1.6 | 37½ | | 1.1 | 1.3 | 1.7 |
| 50 | | 0.9 | 1.3 | 1.6 | 50 | | 1.1 | 1.2 | 1.6 |
| 75 | | 0.9 | 1.4 | 1.7 | 75 | | 0.9 | 1.6 | 1.8 |
| 100 | 0.9 | 1.4 | 1.7 | 100 | 0.9 | 1.4 | 1.7 | | |
| 167 | 0.9 | 1.3 | 1.6 | 167 | 0.9 | 1.3 | 1.6 | | |
| HIGH VOLTAGE 4160/7200Y | | | | | HIGH VOLTAGE 7620/13200Y OR 13200GRDY/7620 | | | | |
| 5 | 120/240 | 2.1 | 1.5 | 2.6 | 5 | 120/240 | 2.2 | 2.2 | 3.1 |
| 10 | | 1.2 | 0.7 | 1.4 | 10 | | 1.4 | 0.8 | 1.6 |
| 15 | | 1.2 | 1.1 | 1.6 | 15 | | 1.3 | 1.2 | 1.8 |
| 25 | | 1.1 | 1.4 | 1.8 | 25 | | 1.2 | 1.6 | 2.0 |
| 37½ | | 0.9 | 1.2 | 1.5 | 37½ | | 1.0 | 1.3 | 1.6 |
| 50 | | 0.9 | 1.3 | 1.6 | 50 | | 1.0 | 1.5 | 1.8 |
| 75 | 0.9 | 1.3 | 1.6 | 75 | 0.9 | 1.6 | 1.8 | | |
| 100 | 0.9 | 1.7 | 1.9 | 100 | 0.9 | 1.6 | 1.8 | | |
| 167 | 0.9 | 1.7 | 1.9 | 167 | 0.9 | 1.7 | 1.9 | | |
| 10 | 240/480 | 1.2 | 0.9 | 1.5 | 10 | 240/480 | 1.4 | 0.9 | 1.6 |
| 15 | | 1.2 | 1.1 | 1.6 | 15 | | 1.3 | 1.0 | 1.6 |
| 25 | | 1.1 | 1.4 | 1.8 | 25 | | 1.2 | 1.4 | 1.9 |
| 37½ | | 1.0 | 1.1 | 1.5 | 37½ | | 1.1 | 1.5 | 1.9 |
| 50 | | 1.0 | 1.3 | 1.6 | 50 | | 1.1 | 1.7 | 2.0 |
| 75 | | 0.9 | 1.3 | 1.6 | 75 | | 0.9 | 1.5 | 1.8 |
| 100 | 0.9 | 1.3 | 1.6 | 100 | 0.9 | 1.5 | 1.7 | | |
| 167 | 0.9 | 1.3 | 1.6 | 167 | 0.9 | 1.5 | 1.8 | | |
| HIGH VOLTAGE 4800/8320Y | | | | | HIGH VOLTAGE 14400/24940GRDY OR 24940GRDY/14400 | | | | |
| 5 | 120/240 | 2.1 | 1.5 | 2.6 | 5 | 120/240 | 2.2 | 2.5 | 3.3 |
| 10 | | 1.2 | 0.9 | 1.5 | 10 | | 1.6 | 1.0 | 1.9 |
| 15 | | 1.2 | 0.9 | 1.5 | 15 | | 1.4 | 1.1 | 1.8 |
| 25 | | 1.1 | 1.4 | 1.8 | 25 | | 1.3 | 1.8 | 2.2 |
| 37½ | | 0.9 | 1.2 | 1.5 | 37½ | | 1.1 | 1.8 | 2.1 |
| 50 | | 0.9 | 1.3 | 1.6 | 50 | | 1.1 | 1.8 | 2.1 |
| 75 | 0.9 | 1.3 | 1.6 | 75 | 1.0 | 2.0 | 2.2 | | |
| 100 | 0.9 | 1.4 | 1.7 | 100 | 1.0 | 2.0 | 2.2 | | |
| 167 | 0.9 | 1.4 | 1.7 | 167 | 1.0 | 2.0 | 2.2 | | |
| 10 | 240/480 | 1.2 | 0.7 | 1.4 | 10 | 240/480 | 1.6 | 1.0 | 1.9 |
| 15 | | 1.2 | 0.9 | 1.5 | 15 | | 1.4 | 1.3 | 1.9 |
| 25 | | 1.1 | 1.5 | 1.9 | 25 | | 1.3 | 1.9 | 2.3 |
| 37½ | | 1.0 | 1.1 | 1.5 | 37½ | | 1.1 | 1.8 | 2.1 |
| 50 | | 1.0 | 1.1 | 1.5 | 50 | | 1.1 | 1.8 | 2.1 |
| 75 | | 0.9 | 1.4 | 1.7 | 75 | | 1.0 | 2.0 | 2.2 |
| 100 | 0.9 | 1.3 | 1.6 | 100 | 1.0 | 1.8 | 2.1 | | |
| 167 | 0.9 | 1.4 | 1.7 | 167 | 1.0 | 1.8 | 2.1 | | |
| 50 | 2400 or 4800 | 1.0 | 1.1 | 1.5 | 50 | 2400 or 4800 | 1.1 | 1.1 | 1.5 |
| 100 | | 0.9 | 1.1 | 1.4 | 100 | | 0.9 | 1.1 | 1.4 |
| 167 | 0.8 | 1.4 | 1.6 | 167 | 0.8 | 1.4 | 1.6 | | |

Table 12—Distribution Transformers—Three-phase Padmount—Single-voltage Primary Maximum Line-to-Line Primary Voltage—25 kV WYE—18 kV Delta

| kVA | Low Voltage | | | | | | kVA | Low Voltage | | | | | |
|------|-------------|------|------|----------|------|------|------|-------------|-------|-------|----------|------|-------|
| | 208Y/120 | | | 480Y/277 | | | | 208Y/120 | | | 480Y/277 | | |
| | %IZ | %IR | %IX | %IZ | %IR | %IX | | %IZ | %IR | %IX | %IZ | %IR | %IX |
| 75 | 1.55 | 1.27 | 0.90 | 1.60 | 1.29 | 0.94 | 300* | 5.25 | 0.95 | 5.70 | 4.95 | 0.88 | 6.29 |
| 75* | 2.70 | 1.34 | 1.29 | 2.90 | 1.37 | 1.35 | 500 | 2.00 | 0.89 | 1.80 | 2.10 | 0.85 | 1.92 |
| 112 | 1.60 | 1.10 | 1.16 | 1.60 | 1.11 | 1.16 | 500* | 5.50 | 0.89 | 6.96 | 5.35 | 0.85 | 7.21 |
| 112* | 3.55 | 1.10 | 2.76 | 3.60 | 1.11 | 2.77 | 750 | 5.75 | 0.93 | 6.56 | 5.75 | 0.88 | 7.32 |
| 150 | 1.95 | 1.08 | 1.63 | 1.90 | 1.11 | 1.55 | 1000 | 5.75 | 0.93 | 6.53 | 5.75 | 0.86 | 7.71 |
| 150* | 4.65 | 1.08 | 3.88 | 4.65 | 1.11 | 3.66 | 1500 | | | | 5.75 | 0.74 | 10.32 |
| 225 | 2.00 | 1.05 | 1.70 | 2.00 | 1.01 | 1.73 | 2000 | | | | 5.75 | 0.70 | 11.82 |
| 225* | 4.65 | 1.09 | 3.85 | 4.75 | 1.06 | 4.13 | 2500 | | | | 5.75 | 0.63 | 14.40 |
| 300 | 2.05 | 1.05 | 1.82 | 2.15 | 0.88 | 1.96 | | | | | | | |

*Original Name Standard

Appendix

Table 13—Transformers for Integral Distribution Centers and Secondary Unit Substations

| kVA | Dry-type | | | | | | Liquid-filled | |
|-------|--------------|------|------------|------|------------|------|----------------------|------|
| | 480V | | 2400-4800V | | 6.9kV-15kV | | 2400-15,000V | |
| | %Z | X/R* | %Z | X/R* | %Z | X/R* | Percent Impedance %Z | X/R |
| 75 | 3.0 | 0.83 | 6.2 | 2.15 | | | | |
| 112.5 | 4.6 | 1.63 | 4.5 | 1.77 | 6.1 | 1.93 | | |
| 150 | 5.5 | 2.08 | 4.2 | 1.95 | 5.3 | 2.33 | | |
| 225 | 5.9 | 4.58 | 4.6 | 1.75 | 6.1 | 2.48 | 2.0† | 2.5* |
| 300 | 4.9 | 2.50 | 5.2 | 3.57 | 6.0 | 3.22 | 4.5† | 3.0* |
| 500 | 6.1 | 3.69 | 5.3 | 4.33 | 6.4 | 4.43 | 4.5† | 3.5* |
| | 2400-15,000V | | | | | | | |
| | | | %Z | X/R | | | | |
| 750 | 5.2 | 2.88 | 5.75 | 5.0 | | | 5.75 | 4.0 |
| 1000 | 4.7 | 3.46 | 5.75 | 5.7 | | | 5.75 | 4.75 |
| 1500 | | | 5.75 | 6.5 | | | 5.75 | 5.5 |
| 2000 | | | 5.75 | 7.2 | | | 5.75 | 5.9 |
| 2500 | | | 5.75 | 7.5 | | | 5.79 | 6.0 |

* Typical ratios based on several manufacturers' data.
† Minimum impedance.

Table 14—Dry-type transformers—Type GHT, % Impedance, Reactance and Resistance (Temp. Base 170°C)†

| kVA | Single-phase | | | Three-phase | | | |
|------|--------------|------|------|-------------|------|------|-----|
| | %IX | %IR | %IZ | kVA | %IX | %IR | %IZ |
| 5 | 1.68 | 2.94 | 3.4 | 6 | 1.72 | 2.72 | 3.2 |
| 7.5 | 1.84 | 2.42 | 3.0 | 9 | 1.16 | 2.31 | 2.6 |
| 10 | 1.92 | 2.04 | 2.75 | 15 | 1.82 | 2.1 | 2.8 |
| 15 | 2.02 | 1.60 | 2.6 | 30 | 1.37 | 3.8 | 4.0 |
| 25 | 2.3 | 1.4 | 2.7 | 45 | 1.73 | 2.52 | 3.1 |
| 37.5 | 2.7 | 3.6 | 4.5 | 75 | 1.91 | 2.27 | 3.0 |
| 50 | 2.8 | 3.1 | 4.2 | 112½ | 3.87 | 2.43 | 4.6 |
| 75 | 3.7 | 2.48 | 4.45 | 150 | 5.0 | 2.35 | 5.5 |
| 100 | 3.55 | 2.12 | 4.14 | 225 | 5.5 | 1.15 | 5.9 |
| 167 | 3.25 | 1.60 | 3.63 | 300 | 4.5 | 1.8 | 4.9 |
| | | | | 500 | 5.9 | 1.6 | 6.1 |

† Typical values based on data from several manufacturers.

Table 15—Standard Current Limiting Reactors

| 600 Volt Insulation Class | | | 5 kV Insulation Class | | 15 kV Insulation Class | |
|---------------------------|-----------------------------------|----------------|------------------------------|----------------|------------------------------|----------------|
| Indoor Service 3φ | | | Single-phase and Three-phase | | Single-phase and Three-phase | |
| Amperes | Fault Δ Current 1 second Duration | OHMS per Phase | Continuous Current Amperes | OHMS per Phase | Continuous Current Amperes | OHMS per Phase |
| 1000 | 23,000 | 0.015 | 200 | 0.25 | 30 | 0.50 |
| 1000 | 34,000 | .010 | | .40 | | .63 |
| 800 | 12,000 | .0285 | 300 | .10 | | 1.0 |
| 800 | 34,000 | .010 | | .16 | | 1.6 |
| | | | | .25 | | 2.5 |
| 600 | 15,000 | .0285 | 400 | .10 | 400 | .40 |
| 600 | 15,000 | .0230 | | .16 | | .50 |
| 600 | 20,000 | .0170 | | .25 | | .63 |
| 600 | 25,000 | .0130 | | | | .80 |
| 600 | 25,000 | .010 | 600 | .063 | | 1.0 |
| 600 | 25,000 | .0046 | | .10 | | 1.6 |
| 400 | 8,000 | .0485 | | .16 | 600 | .25 |
| 400 | 15,000 | .0285 | | .25 | | .40 |
| 400 | 15,000 | .0230 | | | | .50 |
| 400 | 20,000 | .0170 | 1200 | .04 | | .63 |
| 400 | 25,000 | .0130 | | .063 | | .80 |
| 400 | 25,000 | .010 | | .10 | | 1.0 |
| 400 | 25,000 | .0046 | | .16 | | 1.6 |
| 225 | 12,500 | .0285 | 2000 | .04 | 1200 | .16 |
| | | | | .063 | | .25 |
| | | | | .10 | | .40 |
| | | | | | | .50 |
| | | | | | | .63 |
| | | | | | 2000 | .10 |
| | | | | | | .16 |
| | | | | | | .25 |
| | | | | | | .40 |

Δ Maximum allowable sustained symmetrical rms amperes

Table 16—Approximate Machine Reactances LARGE INDUCTION MOTORS

The short-circuit reactance of an induction motor (or induction generator) in percent on its own kVA base may be taken as percent $X''d =$

$$100$$

*times normal stalled rotor current

*with rated voltage and frequency applied.

The reactance of such a machine will generally be approximately (in percent on own kVA base).

| X''d | |
|-------|-------------|
| Range | Most Common |
| 15-25 | 25 |

Table 17—Grouped Small Motors

In many short-circuit studies, the number and size of motors, either induction or synchronous, is not known precisely. However, the short-circuit contribution from these motors must be estimated. In such cases the following table of reactances is used to account for a large number of small induction and synchronous motors.

| Item | Motor Ratings and Corrections | Subtransient Reactance X''d (Percent) | Transient Reactance X'd (Percent) |
|------|--|---------------------------------------|-----------------------------------|
| 1 | 600 volts or less—induction | 25 | — |
| 2 | 600 volts or less—synchronous (items 1 and 2 include motor leads) | 25 | 33 |
| 3 | 600 volts or less—induction | 31 | — |
| 4 | 600 volts or less—synchronous (items 3 and 4 include motor leads and step-down transformers) | 31 | 39 |
| 5 | Motors above 600 volts—induction | 20 | — |
| 6 | Motors above 600 volts—synchronous | 15 | 25 |
| 7 | Motors above 600 volts—induction | 26 | — |
| 8 | Motors above 600 volts—synchronous (items 7 & 8 include step-down transformers) | 21 | 31 |

Table 18—Synchronous Machines Percent Values on Machine kVA Rating

| (A) Generators | X''d | | X'd | |
|---|-------|------|-------|------|
| | Range | Mean | Range | Mean |
| (1) Turbo Generators (distributed pole) | | | | |
| 2 pole, 625-9375 kVA | 6-13 | 9 | | |
| 2 pole, 12,500 kVA-up | 8-12 | 10 | | |
| 4 pole, 12,500 kVA-up | 10-17 | 14 | | |
| (2) Salient-pole Generators (without amortisseur) | | | | |
| 12 poles or less | 15-35 | 25 | | |
| 14 poles or more | 25-45 | 35 | | |
| (3) Salient-pole Generators* (with amortisseur) | | | | |
| 12 poles or less | 10-25 | 18 | | |
| 14 poles or more | 18-40 | 24 | | |
| (B) Synchronous Condensers | 9-38 | 24 | | |
| (C) Synchronous Converters | | | | |
| 600 V dc | 17-22 | 20 | | |
| 250 V dc | 28-38 | 33 | | |
| (D) Synchronous Motors** | | | | |
| 6 pole | 7-16 | 10 | 10-22 | 15 |
| 8-14 pole (incl.) | 11-22 | 15 | 17-36 | 24 |

* Nearly all salient-pole generators built by GE since 1935 have amortisseur windings.
** These data are useful for estimating reactances of individual large motors of several hundred or several thousand horsepower.

Appendix

Feeder Impedance Values Used in Investigation

| Feeder Conductor Size/Phase | Resistance (R) Ohms/Phase/1000 Ft | 60-cycle Inductive Reactance (X) Ohms/Phase/1000 Ft |
|-----------------------------|-----------------------------------|---|
| #4 | .321 | .0483 |
| #1/0 | .128 | .0414 |
| 250 MCM | .055 | .0379 |
| 2-500 MCM | .0147 | .0174 |
| 4-750 MCM | .0054 | .0081 |

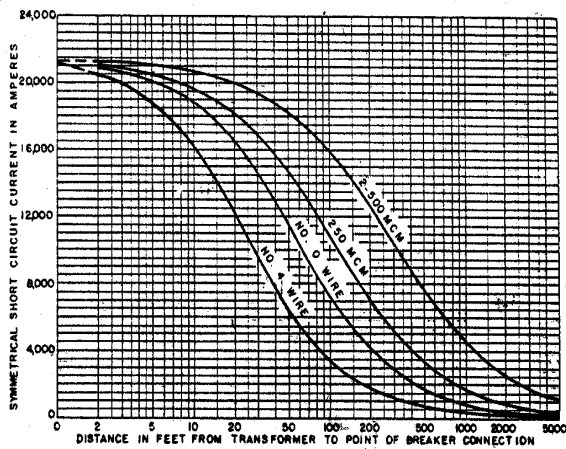


Fig. 25-1. Transf: 150 kVA, 208 V, 2.0% Z

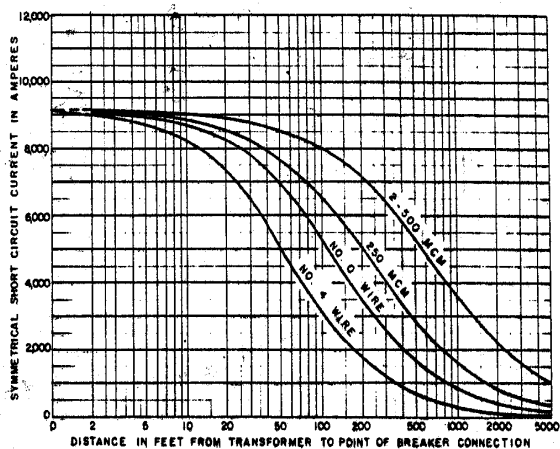


Fig. 25-2. Transf: 150 kVA, 208 V, 4.5% Z

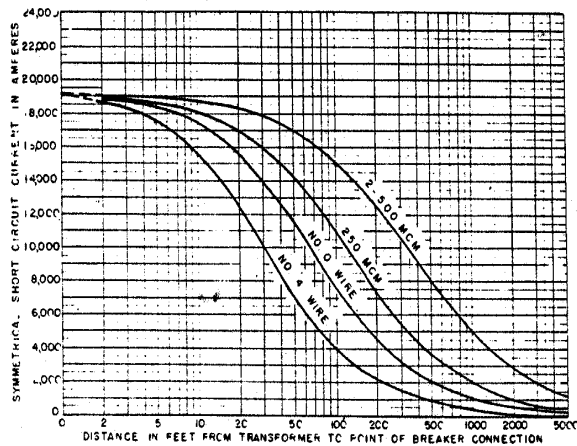


Fig. 25-3. Transf: 150 kVA, 240 V, 2.0% Z

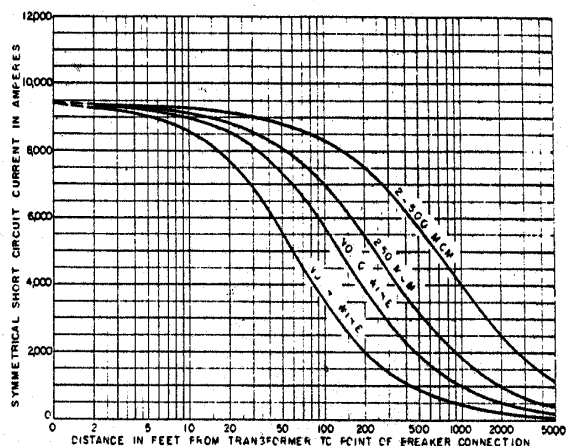


Fig. 25-4. Transf: 150 kVA, 240 V, 4.5% Z

Circuit Breaker Data

| Catalog Number Prefix | No. Poles | Ampere Rating | UL Listed Interrupting Rating—RMS Symmetrical Amperes | | | | | | | | *Federal Specs. W-C 375B/GEN | DP Catalog Class | Digest 162 Page No. |
|-----------------------|-------------|-------------------------------------|---|----------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|--|------------------|---------------------|
| | | | AC Voltage | | | | | | DC Voltage | | | | |
| | | | 120 | 120/240 | 240 | 277 | 277/480 | 480 | 600 | 250 | | | |
| QO-GFI, QOB-GFI | 1 2 | 15-30 15-30 | 10000 10000 | | | | | | | | 11a 10a, 12a | 910 | 3, 78, 80 |
| QO-VHGF, QOB-VHGF | 1 | 15-30 | 22000 | | | | | | | | 11a | 910 | 3, 78, 80 |
| QO-QOB | 1 2 3 | 10-70 10-100 10-60 | 10000 | 10000 | 10000 | | | | | | 10a, 11a, 12a 10a, 12a 10b, 11b, 12b | 730 | 2, 58, 78, 80 |
| QO-H, QOB-H | 2 | 15-30 | | | 10000 | | | | | | 10b, 11b, 12b | 730 | 2, 78, 80 |
| QOT | 1 2 | 15-30 15-30 | 10000 | 410000 10000 | | | | | | | 10a, 11a, 12a 10a, 12a | 731 | 2 |
| QO-VH, QOB-VH | 1 2 3 | 10-30 15-30 15-30 | 22000 | 22000 | 22000 | | | | | | 14a 14a | 730 | 2, 78, 80 |
| QOU | 1 2 3 | 10-70 10-70 10-50 | 10000 | 10000 | 10000 | | | | | | 10a, 12a 10a, 12a 10b, 11b, 12b | 720 | 59 |
| QH-QHB | 1 2 3 | 10-30 15-30 15-30 | 65000 | 65000 | 65000 | | | | | | 15a 15a 15b | 730 | 2, 78, 80 |
| Q1 | 2 3 | 80-150 70-100 | | 10000 | 10000 | | | | | | 10a, 12a 10b, 11b, 12b | 733 | 2, 58, 78 |
| Q1B | 2 3 | 80-100 70-100 | | 10000 | 10000 | | | | | | 10a, 12a 10b, 11b, 12b | 733 | 58, 80 |
| Q1-H, Q1B-H | 2 | 35-100 | | | 10000 | | | | | | 10b, 11b, 12b | 733 | 2, 78, 80 |
| Q1-VH | 2 3 | 35-125 35-100 | | 22000 | 22000 | | | | | | 14a 14b | 733 | 2, 78 |
| Q1B-VH | 2 3 | 35-100 35-100 | | 22000 | 22000 | | | | | | 14a 14b | 733 | 80 |
| Q1H | 2 | 35-125 | | | 42000 | | | | | | 14a | 733 | 2, 78 |
| Q1BH | 2 | 35-100 | | | 42000 | | | | | | 14a | 733 | 80 |
| Q1L | 1 2 3 | 15-100 15-125 15-100 | 10000 | 10000 | 5000 5000 10000 | | | | | | 10a, 12a 10a, 10b, 12a 10b, 11b, 12b | 733 | 59 |
| Q1U | 2 3 | 15-125 15-100 | | 10000 | 5000 10000 | | | | | | 10a, 10b, 12a 10b, 11b, 12b | 733 | 59 |
| Q2 | 2 | 100-225 | | | 10000 | | | | | | | 734 | 95 |
| Q2L | 2 | 100-225 | | | 10000 | | | | | | | 734 | 59 |
| Q2, Q2L | 3 | 100-225 | | | 10000 | | | | | | | 734 | 59, 95 |
| Q2-H, Q2L-H† | 2 3 | 100-225 100-225 | | | 22000 22000 | | | | | | 12b, 14b 12b, 14b | 734 | 59, 95 |
| Q2H, Q2LH | 2 | 100-225 | | | 42000 | | | | | | 12b, 14b | 734 | 59, 95 |
| Q4, Q4L | 2 3 | 250-400 250-400 | | | 22000 22000 | | | | | | 14b 14b | 735 | 59, 95 |
| EH, EHB | 1 2 3 | 15-30 15-60 15-60 | 65000 | 65000 | 65000 | 14000 | 14000 | | | | 11a, 13a 13b, 15a 13b, 15b | 682 | 58, 89 |
| FY | 1 | 15-30 | 18000 | | | 14000 | | | | | 11a, 13a | 651 | 95 |
| FA-FAL 240V. | 1 2 3 | 15-100 15-100 15-100 | 10000 | | 10000 10000 | | | | | | 11a 11b, 12b 11b, 12b | 650 | 60, 95 |
| FA-FAL 480V. | 1 2 3 | 15-100 15-100 15-100 | 18000 | | 18000 18000 | 14000 | 14000 14000 | | | | 11a, 12b, 13a 13b 13b | 650 | 60, 95 |
| FA-FAL 600V. | 2 3 | 15-100 15-100 | | | 18000 18000 | | 14000 14000 | 14000 14000 | | | 18a 18a | 650 | 60, 95 |
| FH-FHL | 1 2 3 | 15-30 35-100 15-100 15-100 | 65000 | | 65000 65000 | 25000 | 25000 18000 | 18000 18000 | | | 13a 13a 22a 22a | 650 | 62, 96 |
| IF-IFL | 2 3 | 20-100 20-100 | | | 100000 100000 | | 100000 100000 | | | | 16a 16a | 820 | 63, 96 |
| KA-KAL | 2 3 | 70-225 70-225 | | | 25000 25000 | | 22000 22000 | 22000 22000 | | | 20a 20a | 655 | 60, 95 |
| KH-KHL | 2 3 | 70-225 70-225 | | | 65000 65000 | | 35000 35000 | 25000 25000 | | | 23a 23a | 655 | 62, 96 |
| IK-IKL | 2 3 | 110-225 110-225 | | | 100000 100000 | | | 100000 100000 | | | 16a 16a | 825 | 63, 96 |
| LA-LAL | 2 3 | 125-400 125-400 | | | 42000 42000 | | 30000 30000 | 22000 22000 | | | 21a 21a | 660 | 61, 95 |
| LH-LHL | 2 3 | 125-400 125-400 | | | 65000 65000 | | 35000 35000 | 25000 25000 | | | 23a 23a | 660 | 62, 96 |
| IL-ILL | 3 | 250-400 | | | 100000 | | | 100000 | | | | 830 | 63, 96 |
| MA-MAL | 2 3 | 125-1000 125-1000 | | | 42000 42000 | | 30000 30000 | 22000 22000 | | | 21a 21a | 665 | 61, 95 |
| MH-MHL | 2 3 | 125-1000 125-1000 | | | 65000 65000 | | 50000 50000 | 25000 25000 | | | 23a 23a | 665 | 62, 96 |
| ME-MEL | 2 3 | 125-800 125-800 | | | 65000 65000 | | 50000 50000 | 25000 25000 | | | 23a 23a | 666 | 64, 97 |
| NHL | 2 3 | 600-1200 600-1200 | | | 65000 65000 | | 50000 50000 | | | | 23a 23a | 670 | 61 |
| PAF | 2 3 | 600-2000 600-2000 | | | 65000 65000 | | 50000 50000 | 42000 42000 | | | 24a 24a | 675 | 61 |
| PHF | 2 3 | 600-2000 600-2000 | | | 125000 125000 | | 100000 100000 | 65000 65000 | | | 25a 25a | 675 | 62 |
| PEF, PEC † | 2 3 | 1000-2000 1000-2000 | | | 125000 125000 | | 100000 100000 | 65000 65000 | | | 25a 25a | 677 | 65 |
| PCF | 2 3 | 1600-2800 1600-2800 | | | 125000 125000 | | 100000 100000 | 65000 65000 | | | 25a 25a | 676 | 61 |

*Federal Specs. do not require dc ratings.
 †125V. dc.
 ‡QOT 1515, QOT 1520 and QOT 2020 rated 120V. ac.
 †2 Pole rated 10,000 AIC, 240V., 3Ø, Grd. BØ.
 ●QO only. QOB maximum rating 70 amperes.