

Computer Vision and Measurements in Aerospace Applications

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Objective

To build a unified theoretical framework for quantitative image-based measurements of morphology and motion fields of deformable bodies like fluids

- *Geometric Structures:*
Points, Curves, Surfaces
- *Motion Fields:*
Points, Curves, Surfaces (Geometric Flow)
Complex Continuous Patterns

Background

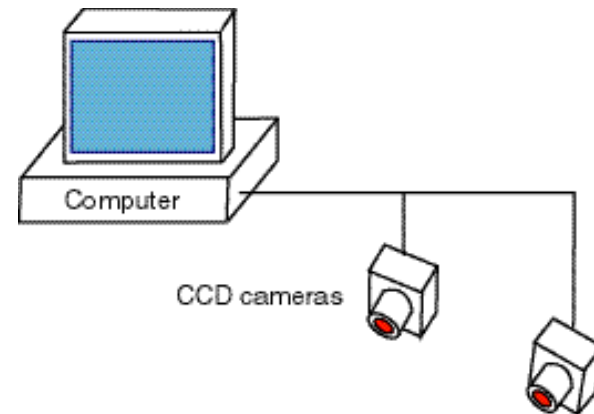
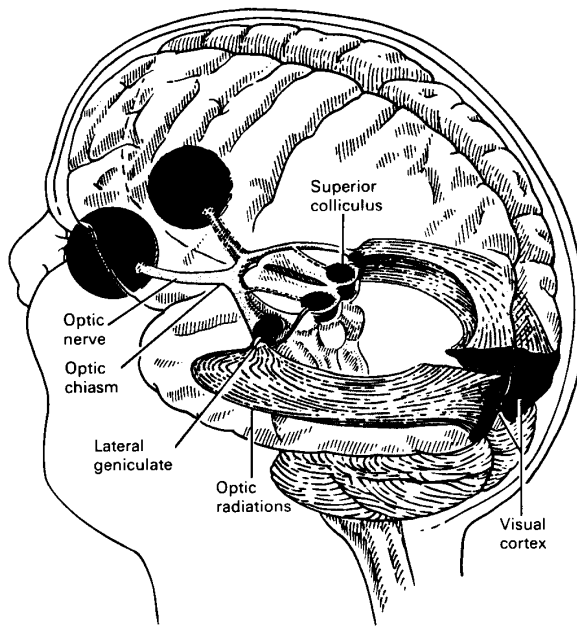
- **Photogrammetry**
- **Computer Vision**

Human Vision

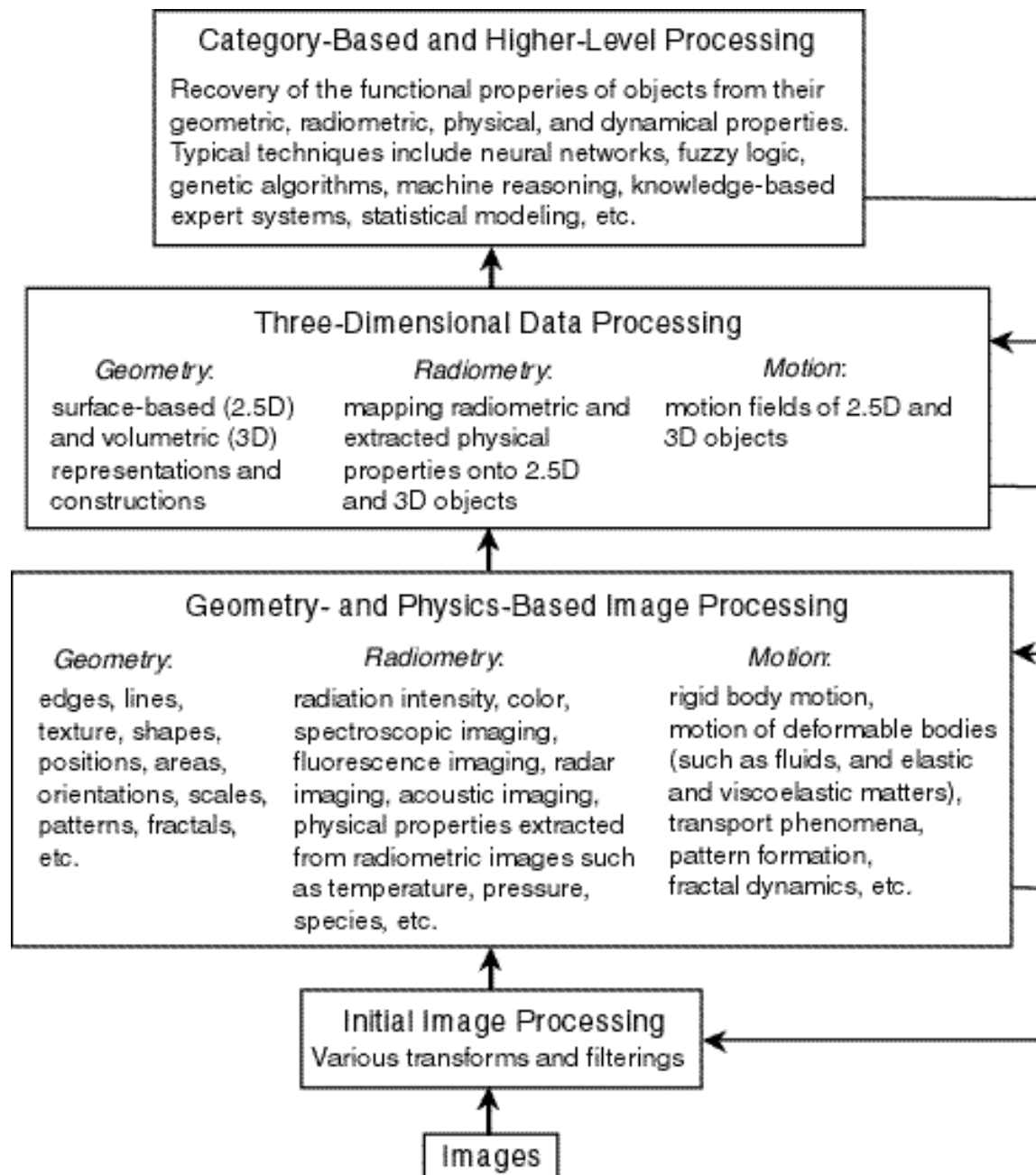


Computer Vision

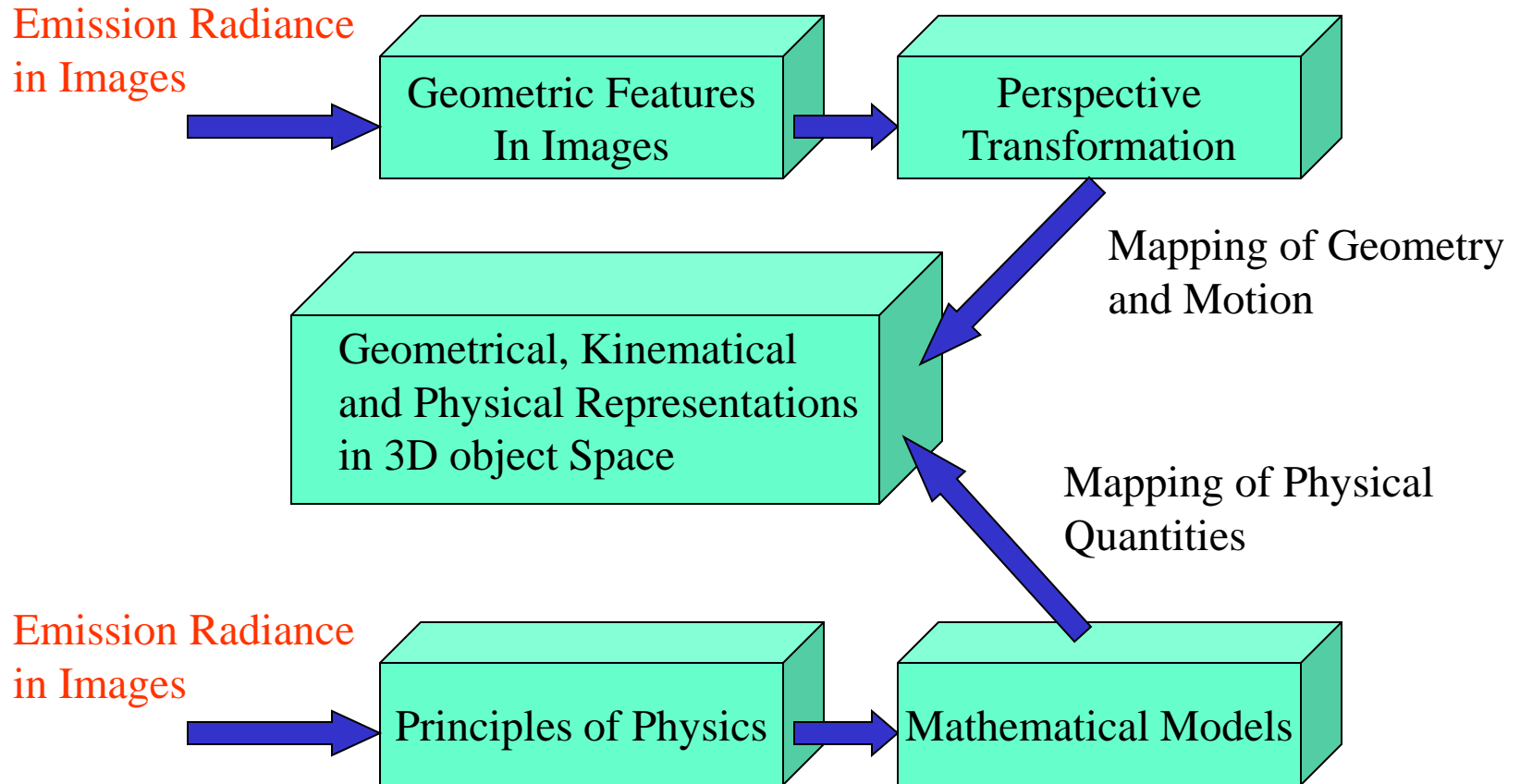
Analogy



Optical Info Processing

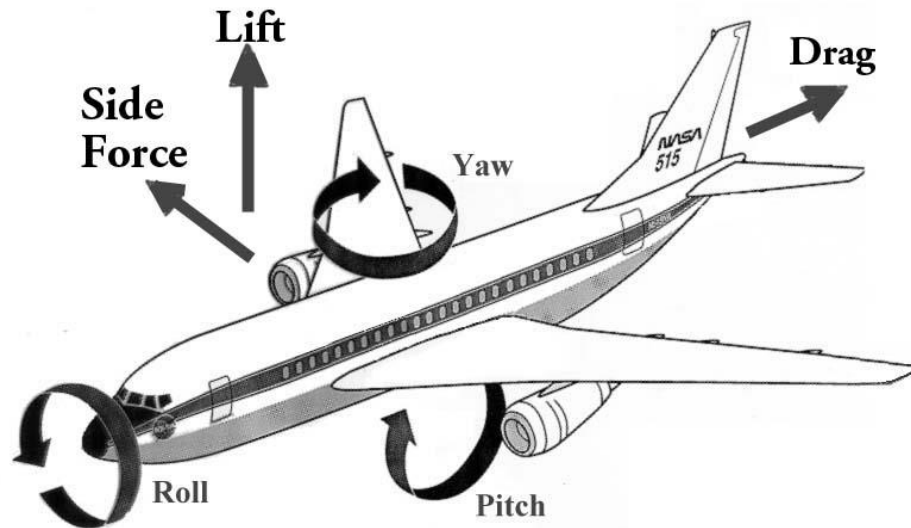


Geometric and Physical-Based Processing



Important Quantities in Aerodynamics

- (1) Pressure
- (2) Temperature
- (3) Skin Friction
- (4) Velocity Field
- (5) Attitude and Kinematics
- (6) Shape



Molecular Sensors!

Needs for New Methods

*Quantitative, Dynamic, Universal, Applicable
to Complex Patterns & Motions of Deformable
Bodies*

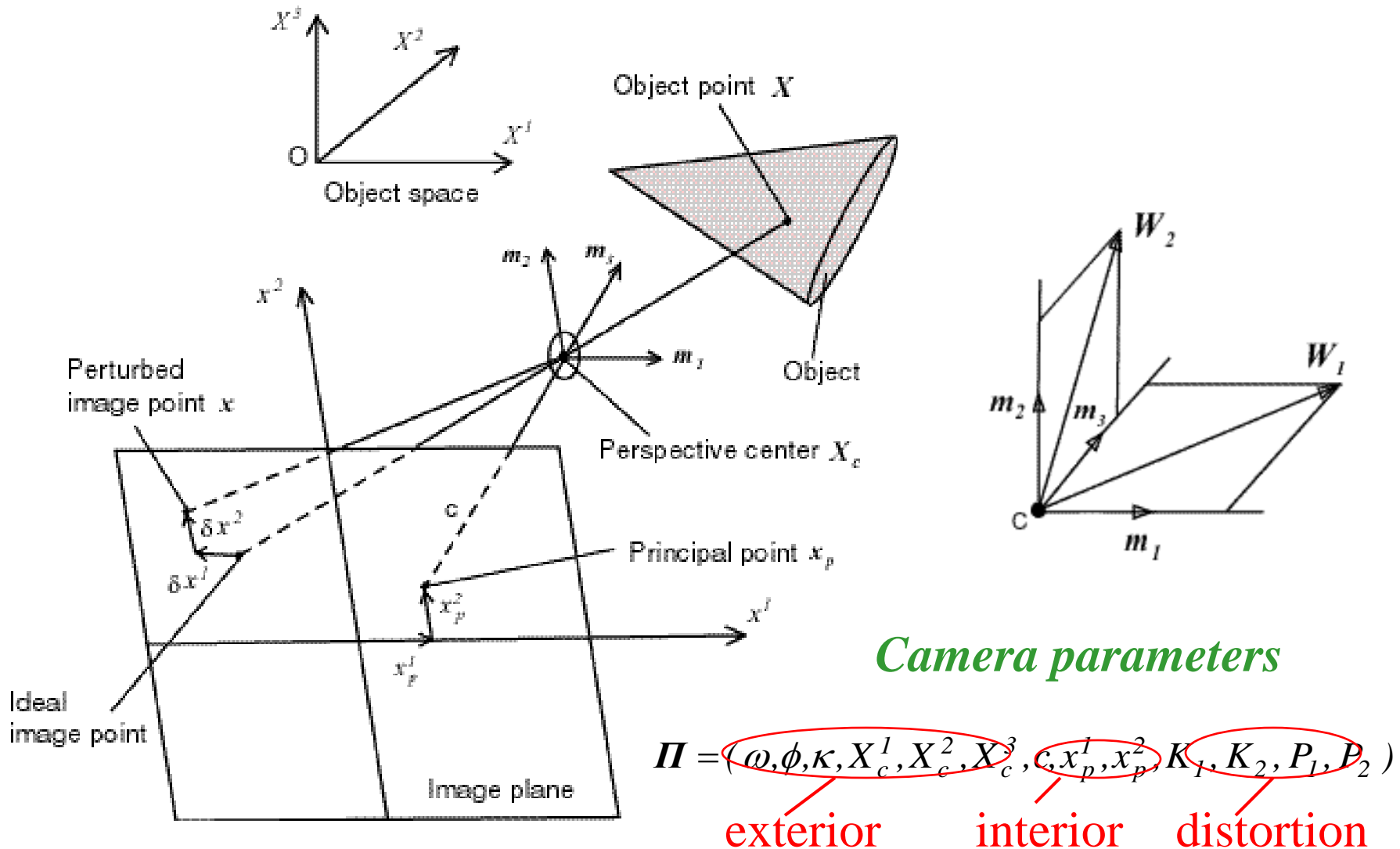
Combination of Approaches

- *Perspective Geometry*
- *Differential Geometry*
- *Continuum Kinematics & Dynamics*
- *Radiometry*

Relevant Topics

- (1) *Perspective Projection Transformation*
- (2) *Projective Developable Conical Surface*
- (3) *Perspective Projection under Surface Constraint*
- (4) *Perspective Projection of Motion Field
Constrained on Surface*
- (5) *The Correspondence Problem*
- (6) *Composite Image Space and Object Space*
- (7) *Perspective Invariants of 3D Curve*
- (8) *Reflection and Shape Recovery*
- (9) *Motion Equations of Image Intensity*

Perspective Projection Transformation



Formulations of Perspective Transformation

(1) Collinearity Equations

$$x^1 - x_p^1 + \delta x^1 = -c \frac{\mathbf{m}_1^T (\mathbf{X} - \mathbf{X}_c)}{\mathbf{m}_3^T (\mathbf{X} - \mathbf{X}_c)}$$

$$x^2 - x_p^2 + \delta x^2 = -c \frac{\mathbf{m}_2^T (\mathbf{X} - \mathbf{X}_c)}{\mathbf{m}_3^T (\mathbf{X} - \mathbf{X}_c)}$$

(2) Homogenous Coordinate Form

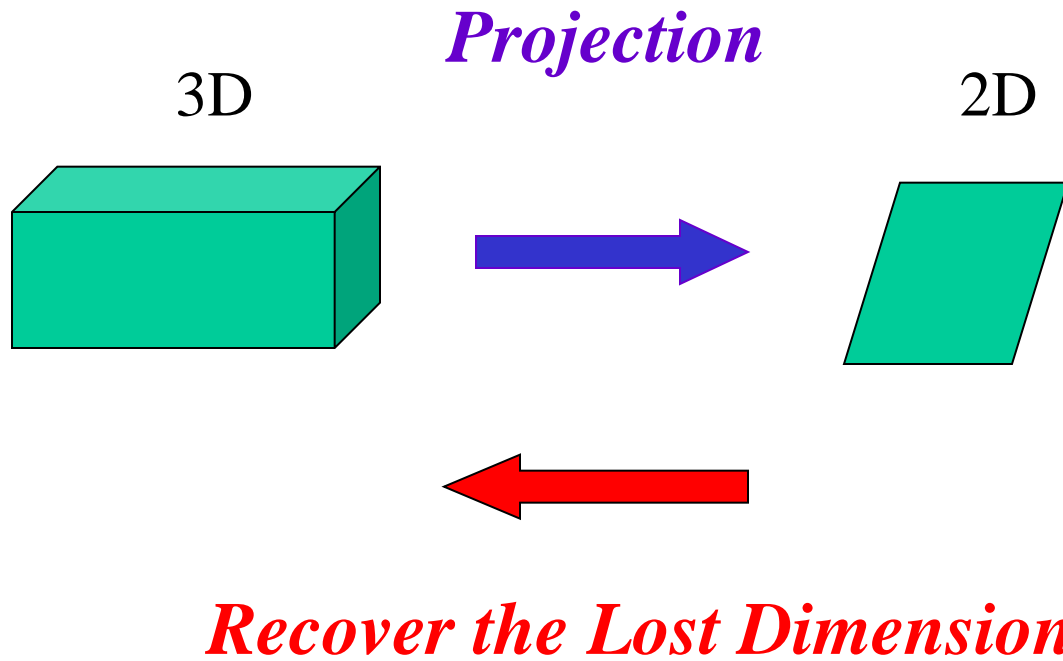
$$\mathbf{x}_h = \lambda \mathbf{P}_h \mathbf{X}_h$$

(3) W-Vector Form

$$\mathbf{W}_1^T (\mathbf{X} - \mathbf{X}_c) = 0$$

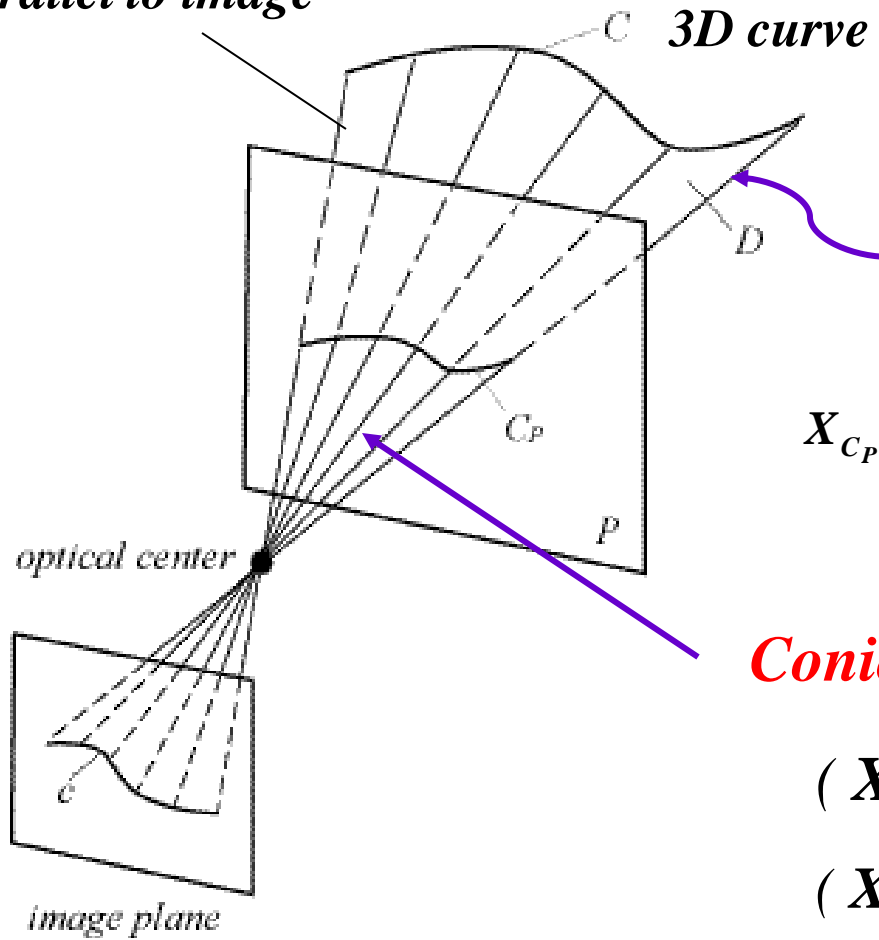
$$\mathbf{W}_2^T (\mathbf{X} - \mathbf{X}_c) = 0$$

Geometric Image Measurements



Perspective Developable Conical Surface

Plane parallel to image



Ray Equation

$$\mathbf{X}_{C_P} - \mathbf{X}_c = \lambda^{-1} (\bar{\mathbf{P}} \mathbf{x}_{h0} + \int_0^s \bar{\mathbf{P}}_{32} \mathbf{t} ds)$$

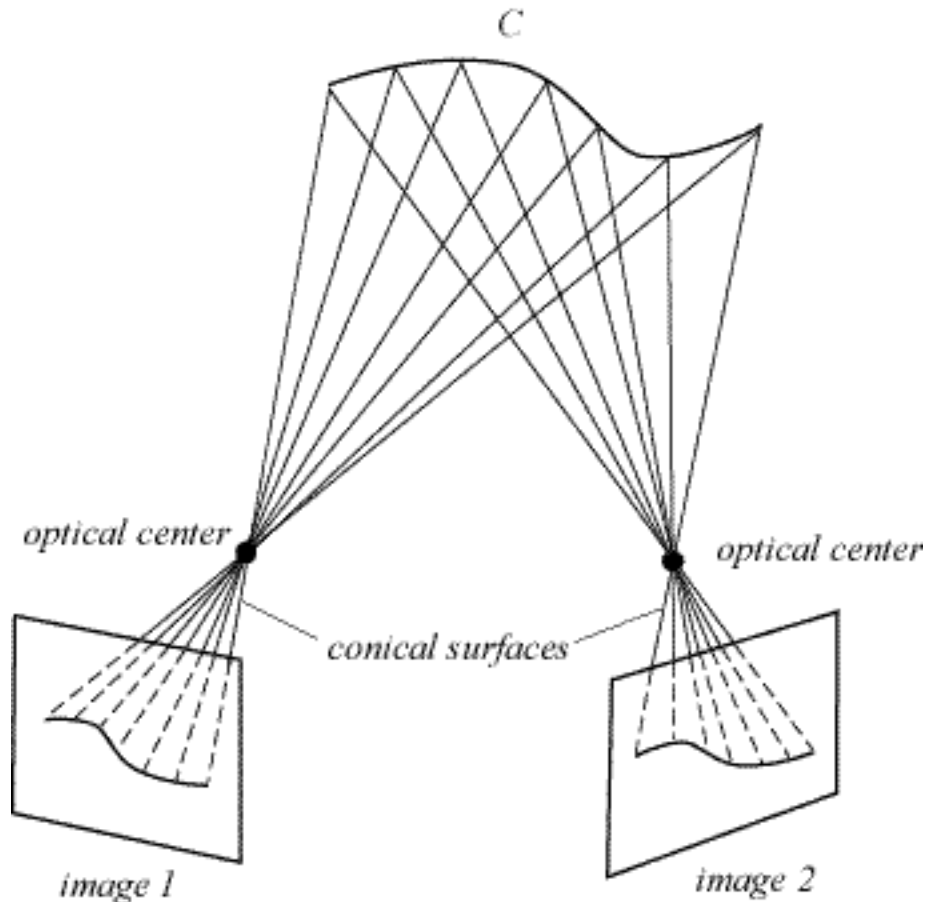
Conical Surface Equations

$$(\mathbf{X} - \mathbf{X}_c) \cdot \mathbf{N}_D(s) = 0$$

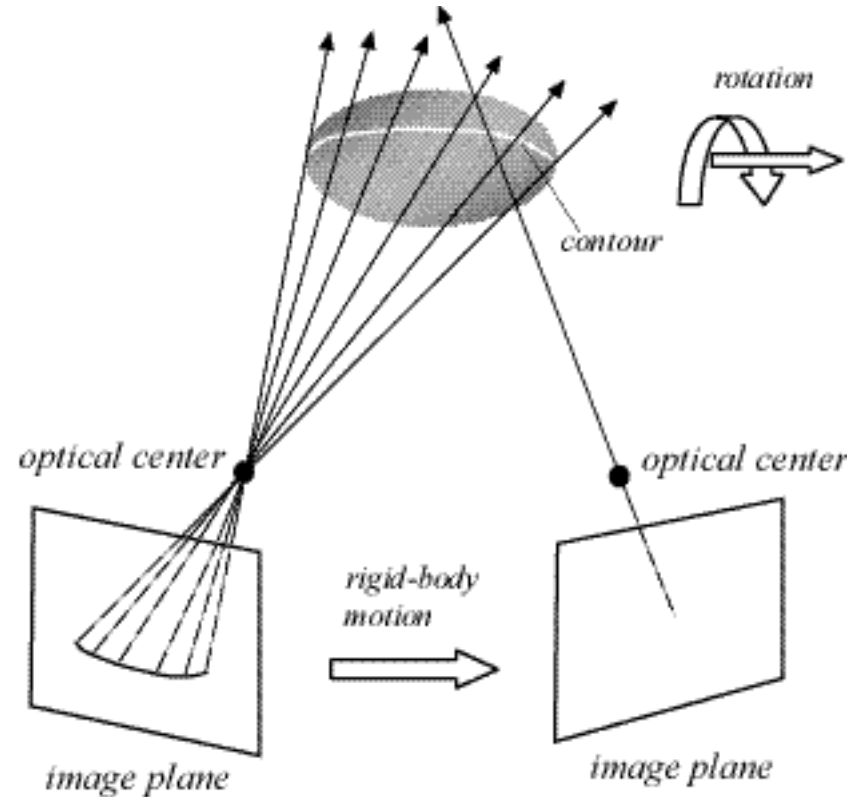
$$(\mathbf{X} - \mathbf{X}_c) \cdot d\mathbf{N}_D(s) / ds = 0$$

Reconstruction of 3D Curves and Surfaces Using Projective Conical Surfaces

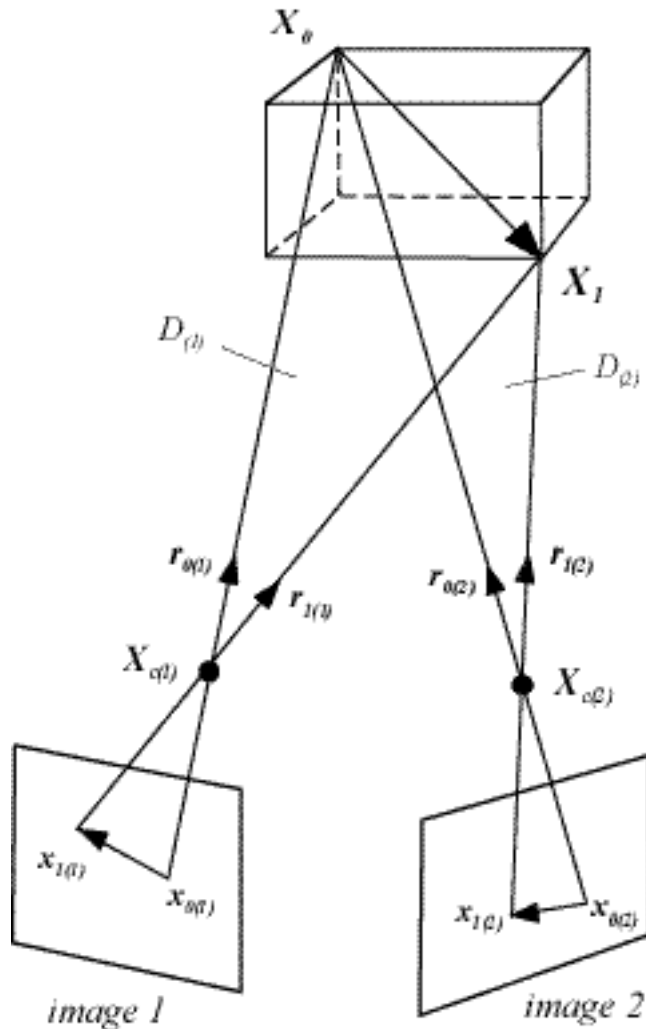
3D Space Curve



Surface

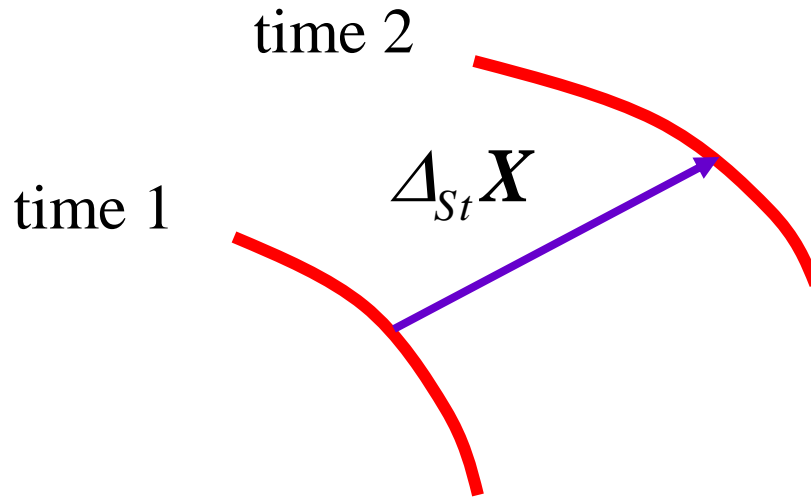


Reconstruction of 3D Displacement Vectors



Providing a rational and general method for Stereoscopic Particle Image Velocimetry (SPIV) and Scalar Image Velocimetry (SIV)

Motion Field of 3D Space Curve



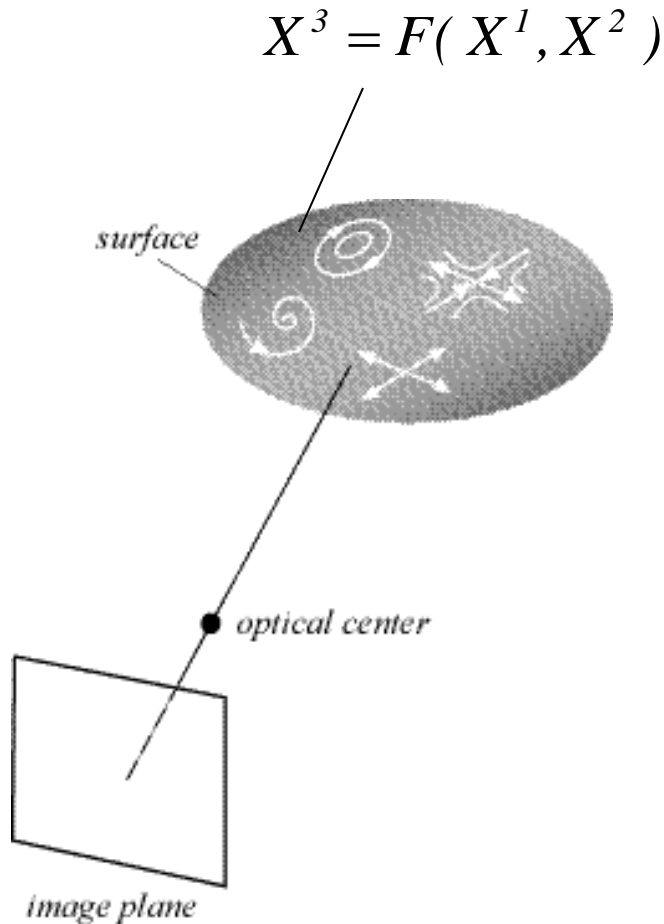
Variational Problem:

$$\| \Delta_{St} \mathbf{X} - \mathbf{U}(\mathbf{X}) \Delta t \| \rightarrow \min$$

Physical and Geometric Constraints:

$$G_i[\mathbf{U}(\mathbf{X})] = 0 \quad i = 1, 2, \dots$$

Perspective Projection under Surface Constraint



One-to-One Differential Relation

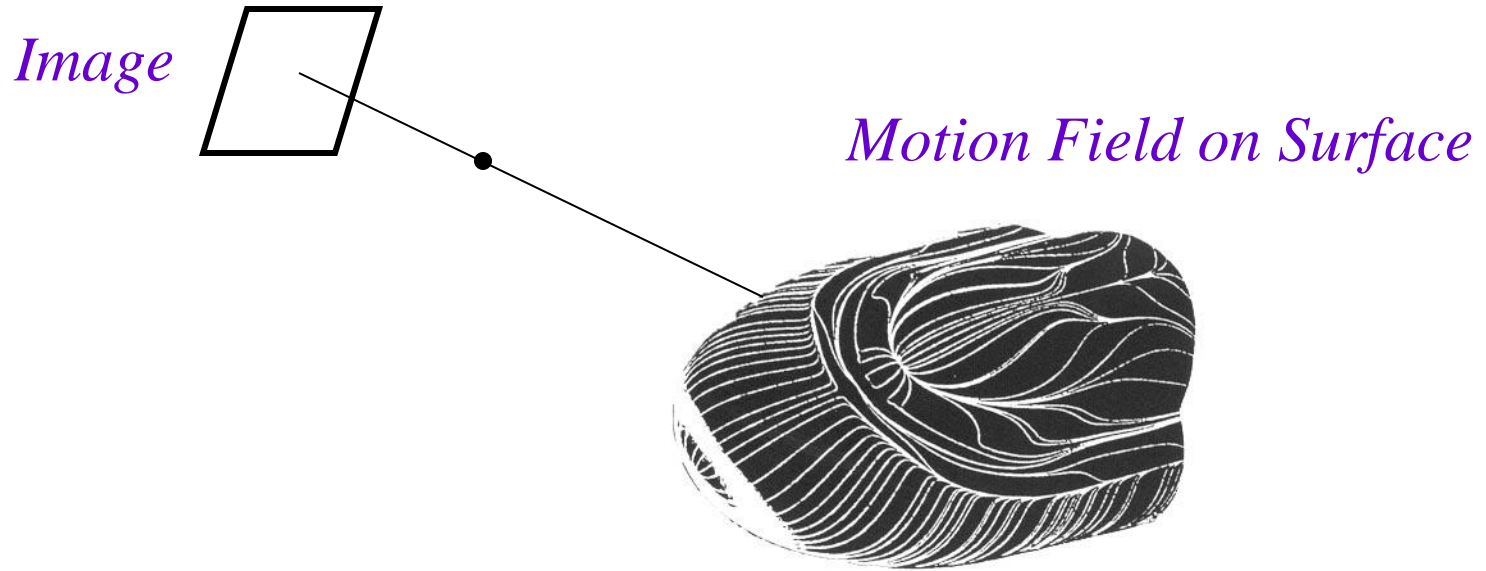
$$\begin{pmatrix} dX^1 \\ dX^2 \end{pmatrix} = \mathbf{m}_3^T (\mathbf{X}_c - \mathbf{f}_s) \mathbf{Q}^{-1} \begin{pmatrix} dx^1 \\ dx^2 \end{pmatrix}$$

Geometric Structures

$$dS^2 = |d\mathbf{X}| = g_{\alpha\beta} dx^\alpha dx^\beta$$

Quantities: tangents, normal, length, angle, area topology

Surface-Constrained Motion Field

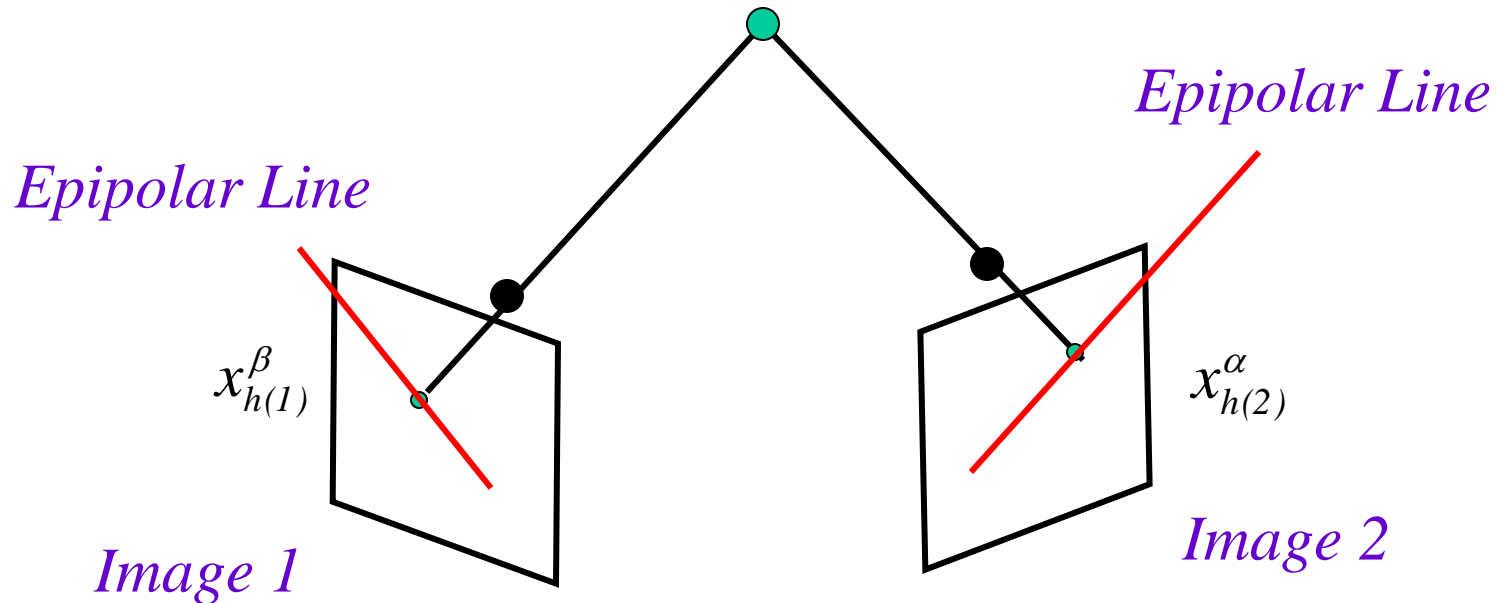


$$\mathbf{u} = \frac{d}{dt} \begin{pmatrix} x^1 \\ x^2 \end{pmatrix} = \frac{Q}{\mathbf{m}_3^T (\mathbf{X}_c - \mathbf{f}_s)} \begin{pmatrix} U_1[\mathbf{f}_s(\mathbf{x})] \\ U_2[\mathbf{f}_s(\mathbf{x})] \end{pmatrix}$$

Optical Flow

Motion Field

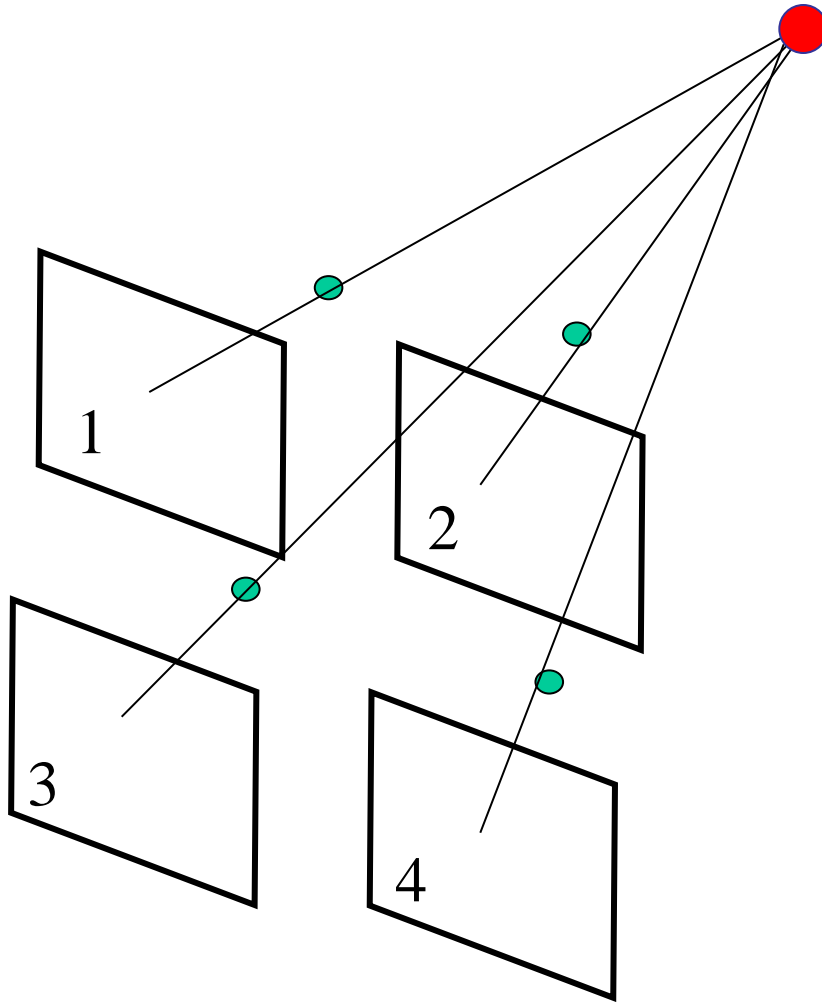
The Point Correspondence Problem



Generalized Longuet-Higgins Relation:

$$(x_{h(2)}^\alpha + \delta x_{h(2)}^\alpha) Q_{\alpha\beta} (x_{h(1)}^\beta + \delta x_{h(1)}^\beta) = 0$$

Determining Point Correspondence

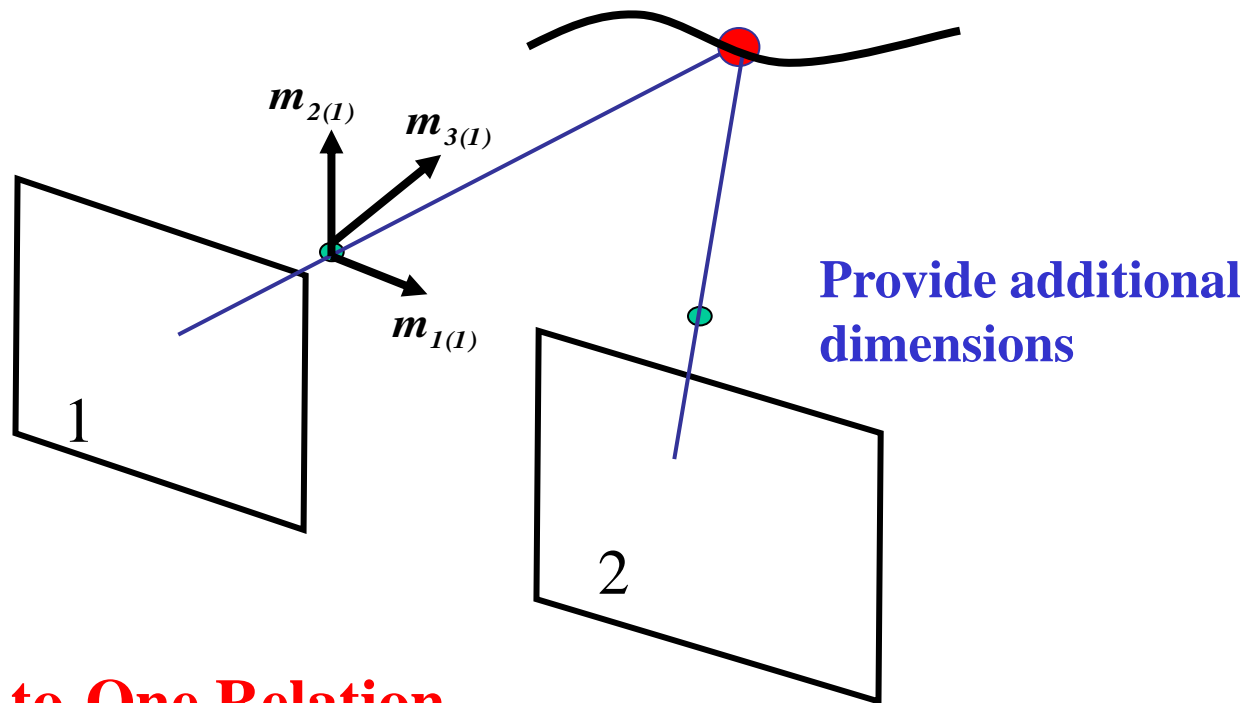


Four Images or Cameras

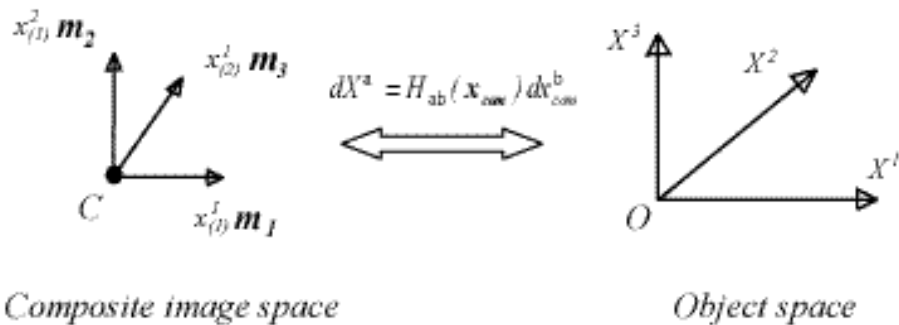


*Six Longuet-Higgins
Equations
for
Six Unknowns*

Composite Image Space and Object Space



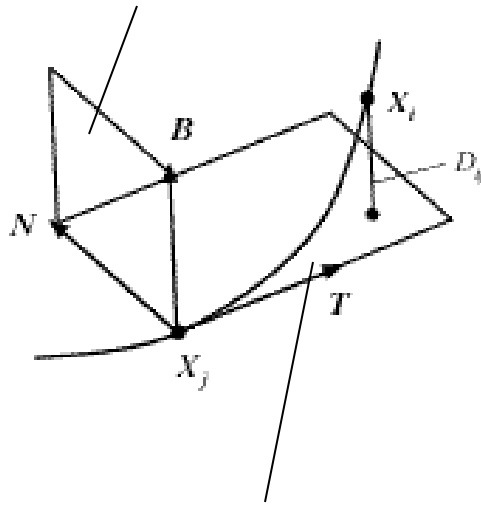
One-to-One Relation



Reconstruct 3D
Displacement Vectors
from Composite Image
Coordinates

Perspective Invariants of 3D Curve

Rectifying plane



Osculating plane

Torsion

$$\frac{\tau_{im,1} d_{12}^2}{\tau_{im,2} d_{21}^2} = \frac{\tau_{obj,1} D_{12}^2}{\tau_{obj,2} D_{21}^2}$$

new

Curvatures

$$\frac{\kappa_{im,2} d_{12} i^2(1,1',2,3)}{\kappa_{im,1} d_{21} i^2(1,2,2',3)} = \frac{\kappa_{obj,2} D_{12} I^2(1,1',2,3)}{\kappa_{obj,1} D_{21} I^2(1,2,2',3)}$$

new

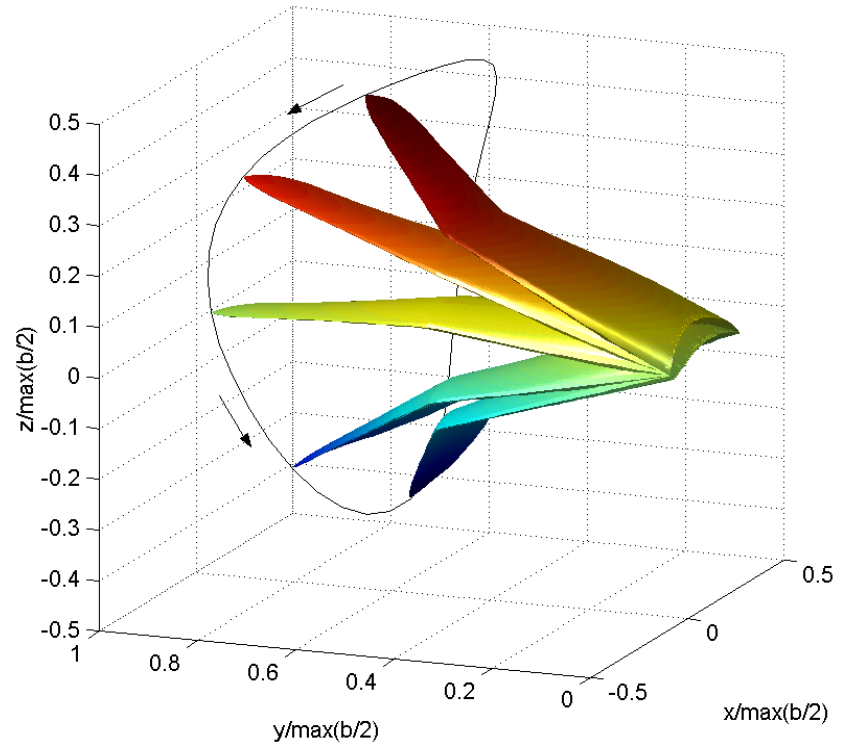
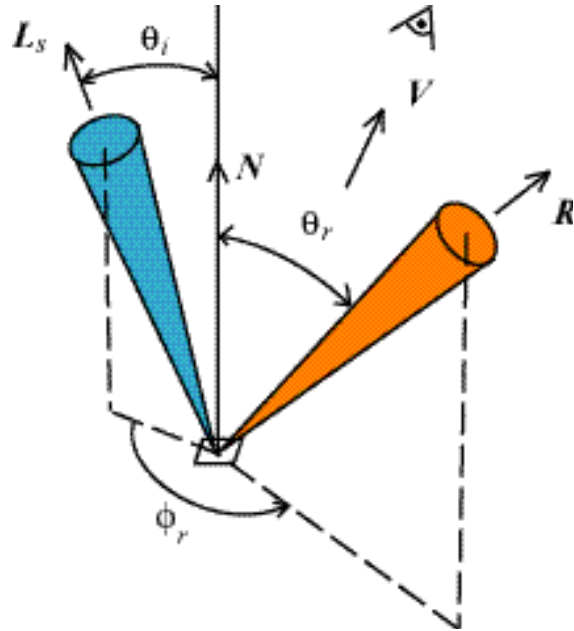
Distances

$$\frac{d_{21} d_{43}}{d_{41} d_{23}} = \frac{D_{21} D_{43}}{D_{41} D_{23}}$$

(Brill, et al. 1992)

Geometrical Flow Problem

Shape and Reflection



$$I(\mathbf{x}) = c_{\text{sys}} \rho_a E_a$$

$$+ c_{\text{sys}} E_{ls} [\rho_d \mathbf{N} \cdot \mathbf{L}_s + \rho_s p (a_N \mathbf{N} \cdot \mathbf{V} + a_L \mathbf{L}_s \cdot \mathbf{V})]$$

Motion Equations of Image Intensity

Image Intensity and Radiance

$$I(\mathbf{x}, t) = c L(\mathbf{X}, \mathbf{a}, \mathbf{g}, t)$$

Physical parameters: $\mathbf{p} = (p_1, p_2, \dots, p_N)^T$

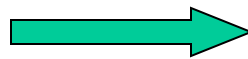
Geometric parameters: $\mathbf{q} = (q_1, q_2, \dots, q_M)^T$

Radiance: $L(\mathbf{X}, \mathbf{p}, \mathbf{q})$

Generic Motion Equations of Image Intensity

$$\frac{\partial I}{\partial t} + \mathbf{u} \cdot \nabla_x I = c_{sys} \left(\frac{\partial L}{\partial t} + \mathbf{U} \cdot \nabla_X L + \frac{d\mathbf{p}}{dt} \cdot \nabla_p L + \frac{d\mathbf{q}}{dt} \cdot \nabla_q L \right)$$

Optical Flow



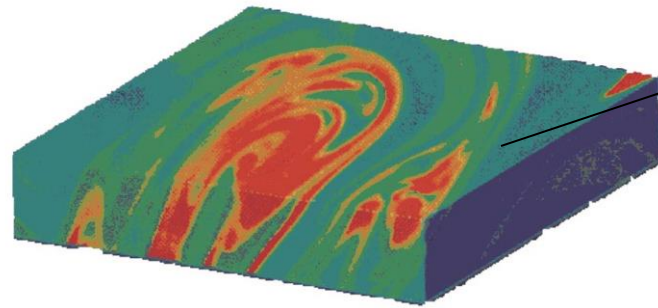
Velocity Field

Physical parameters: $\mathbf{p} = (p_1, p_2, \dots, p_N)^T$

Geometric parameters: $\mathbf{q} = (q_1, q_2, \dots, q_M)^T$

Radiance: $L(X, p, q)$

Emitting Passive Scalar Transport



Luminescence

Governing Equation

Radiance

$$\frac{d\psi}{dt} = \frac{\partial\psi}{\partial t} + \mathbf{U} \cdot \nabla \psi = D_{\psi} \nabla_{\mathbf{X}}^2 \psi$$

$$L(\mathbf{X}, t) = c_{\psi} \psi(\mathbf{X}, t)$$

Perspective Projection onto Image Plane

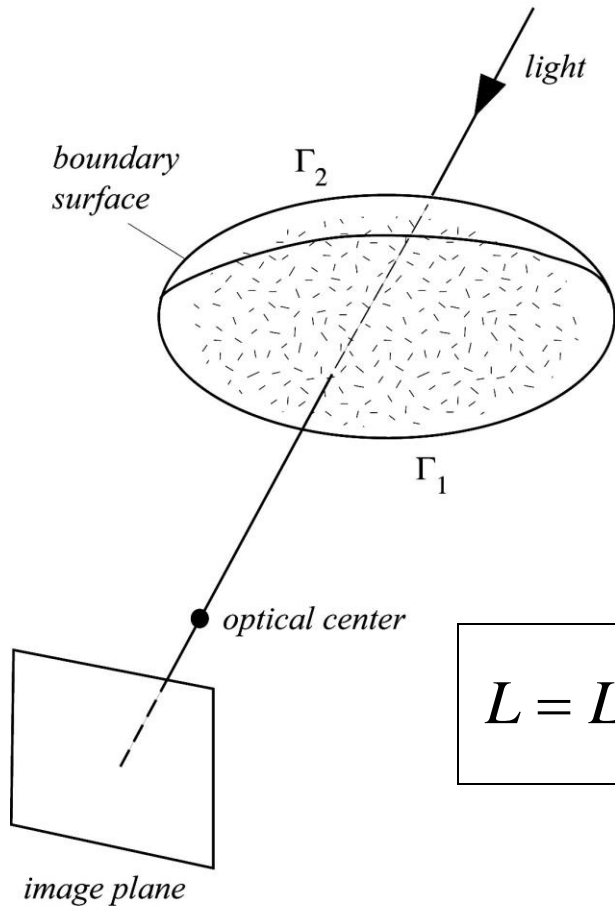
Motion Equation of Image Intensity for Emitting Passive Scalar Transport

$$\frac{\partial I}{\partial t} + u_{\alpha} \frac{\partial I}{\partial x^{\alpha}} = D_{\psi} \left(h_{\lambda} \frac{\partial I}{\partial x^{\lambda}} + h_{\lambda\alpha} \frac{\partial^2 I}{\partial x^{\alpha} \partial x^{\lambda}} \right)$$

Optical Flow and Velocity Field on Surface

$$\mathbf{u} = \frac{d}{dt} \begin{pmatrix} x^1 \\ x^2 \end{pmatrix} = \frac{\mathbf{G}}{\mathbf{m}_3 \cdot (\mathbf{X}_c - \mathbf{f}_s)} \begin{pmatrix} U_1[\mathbf{f}_s(\mathbf{x})] \\ U_2[\mathbf{f}_s(\mathbf{x})] \end{pmatrix}$$

Light Transmitting Scalar Transport



Governing Equation

$$\frac{d\psi}{dt} = \frac{\partial\psi}{\partial t} + \mathbf{U} \cdot \nabla\psi = D_{\psi} \nabla_X^2 \psi$$

$$L = L_0 \exp\left(-\int_0^s \beta_{ext} ds\right)$$

Perspective Projection onto Image Plane

Motion Equation of Image Intensity for Light Transmitting Scalar Transport

$$\frac{\partial I}{\partial t} + u_{\beta} \frac{\partial I}{\partial x^{\beta}} = D_{\psi} \lambda^2 \left(\frac{\partial^2 I}{\partial x^{\beta} \partial x^{\beta}} - I^{-1} \frac{\partial I}{\partial x^{\beta}} \frac{\partial I}{\partial x^{\beta}} \right)$$

Optical Flow and Path-Averaged Velocity

$$u_{\alpha} \frac{\partial I}{\partial x^{\alpha}} = \langle \mathbf{U}_{12} \rangle_{\psi} \cdot \nabla_{12} I$$

where

$$\langle \mathbf{U}_{12} \rangle_{\psi} = \frac{\int_{\Gamma_1}^{\Gamma_2} \psi \mathbf{U}_{12} d\bar{X}^3}{\int_{\Gamma_1}^{\Gamma_2} \psi d\bar{X}^3}$$

Schlieren Image of Density-Varying Flows

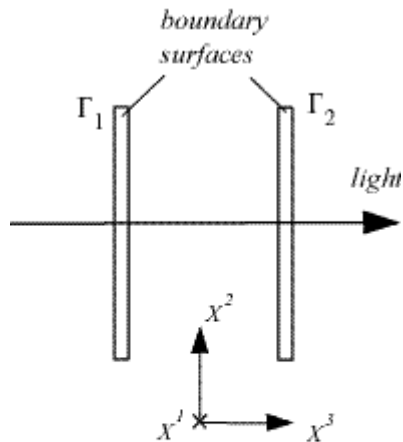


Image Intensity and Density Gradient

$$\frac{I - I_K}{I_K} = C_{schl} \int_{\Gamma_1}^{\Gamma_2} \frac{\partial \rho}{\partial X^2} dX^3$$

Motion Equations of Image Intensity

$$\frac{\partial}{\partial t} \int_{X_0^2}^{X^2} (I - I_K) dX^2 + \nabla_{12} \cdot [\langle \mathbf{U}_{12} \rangle_{\rho} \int_{X_0^2}^{X^2} (I - I_K) dX^2] = 0$$

where $\langle \mathbf{U}_{12} \rangle_{\rho} = \frac{\int_{\Gamma_1}^{\Gamma_2} \rho \mathbf{U}_{12} d\bar{X}^3}{\int_{\Gamma_1}^{\Gamma_2} \rho d\bar{X}^3}$ $\nabla_{12} = (\partial / \partial X^1, \partial / \partial X^2)^T$

Shadowgraph Image of Density-Varying Flows

Image Intensity and Second-Order Density Derivative

$$\frac{I - I_T}{I_T} = C_{shad} \int_{\Gamma_1}^{\Gamma_2} \nabla_{12}^2 \rho dX^3$$

Motion Equations of Image Intensity

$$\frac{\partial}{\partial t} \nabla_{12}^{-2} (I - I_T) + \nabla_{12} \cdot [\langle \mathbf{U}_{12} \rangle_{\rho} \nabla_{12}^{-2} (I - I_T)] = 0$$

where $\nabla_{12}^2 \phi = I - I_T$ *solution* $\longrightarrow \nabla_{12}^{-2} (I - I_T)$

Transmittance Image of Density-Varying Flows

Image Intensity and Density

$$\frac{I - I_T}{I_T} = C_{trans} \int_{\Gamma_1}^{\Gamma_2} \rho dX^3$$

Motion Equations of Image Intensity

$$\frac{\partial}{\partial t} (I - I_T) + \nabla_{12} \cdot [\langle \mathbf{U}_{12} \rangle_{\rho} (I - I_T)] = 0$$

Typical Applications

- Aerodynamic measurements: pressure and temperature sensitive paints, videogrammetric attitude measurement, stereoscopic PIV, laser-tagging technique, schlieren, shadow and transmittance imaging, oil-film/liquid-crystal skin friction measurements.
- Metrology and kinematics of large inflatable space structure.

Unification of Measurement Systems

Conventional Techniques

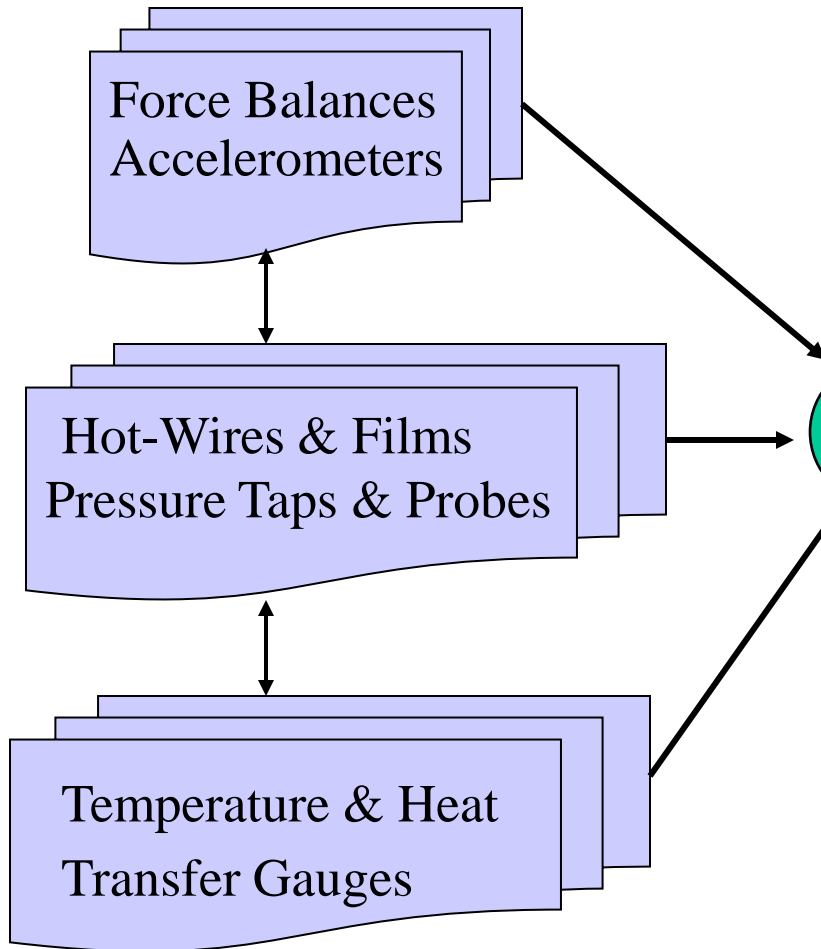
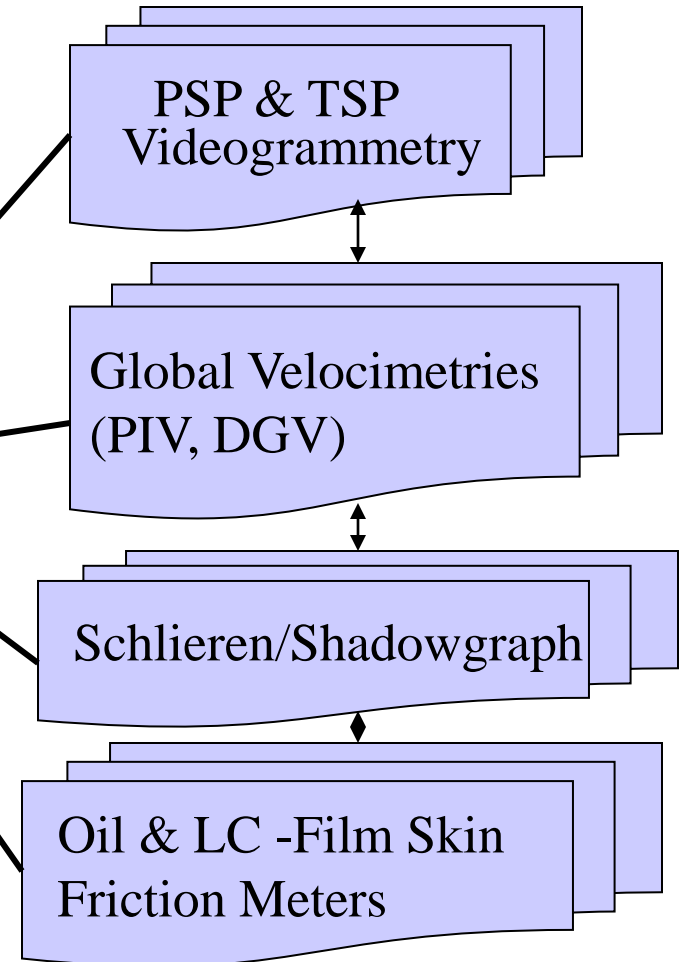


Image-Based Techniques



Data Fusion and Understanding

Measurements

Integrated data & data
at discrete locations

Distributions on surfaces

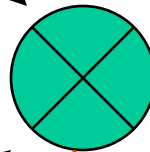
Fields in 3D space

Data Base & Models

Aerodynamics
data base

Theoretical models

CFD



***“SuperAerodynamicist”:
Intelligent Expert System!?”***

Conclusions

We will see unified image-based instrumentation providing non-contact, global measurements of important physical, geometric and dynamical quantities in wind tunnel testing.

Ideal Aerodynamics Lab

